



Membrane-based Absorption Heat Pump Water Heaters

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Outline

- Motivation
- Operation principle
 - Closed & open absorption cycle water heaters
- Membrane-based absorption cycle
 - Theory and experiments
 - Preliminary system level tests
- Ionic liquids (ILs) for absorption cycles
 - Unique properties and prospects
- Summary

Motivation

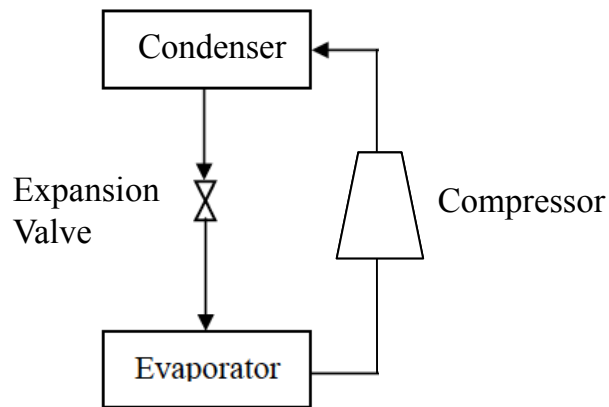
➤ ~50% of the water heaters shipped are gas-fired

Residential	2009	2010
Gas Storage (Total)	3,760,657	3,918,510
<i>Not E*¹⁷</i>	3,110,419	3,463,780
<i>E*-qualifying¹⁸</i>	650,238	454,730
Gas Tankless (Total)¹⁹	380,000	399,000²⁰
<i>Not E*</i>	46,987	14,974
<i>E*-qualifying</i>	333,013	384,026
Electric Storage (Total)	3,751,994	3,736,597
<i>Not E*²¹</i>	3,737,260	3,677,472
<i>E*-qualifying (heat pump)²²</i>	14,734	59,125
Solar²³	31,647	33,462
<i>Not E*</i>	24,751	23,472
<i>E*-qualifying</i>	6,896	9,990
TOTAL	7,924,298	8,087,569
<i>Total Not E*</i>	6,919,417	7,179,698
<i>Total E* qualifying</i>	1,004,881	907,871

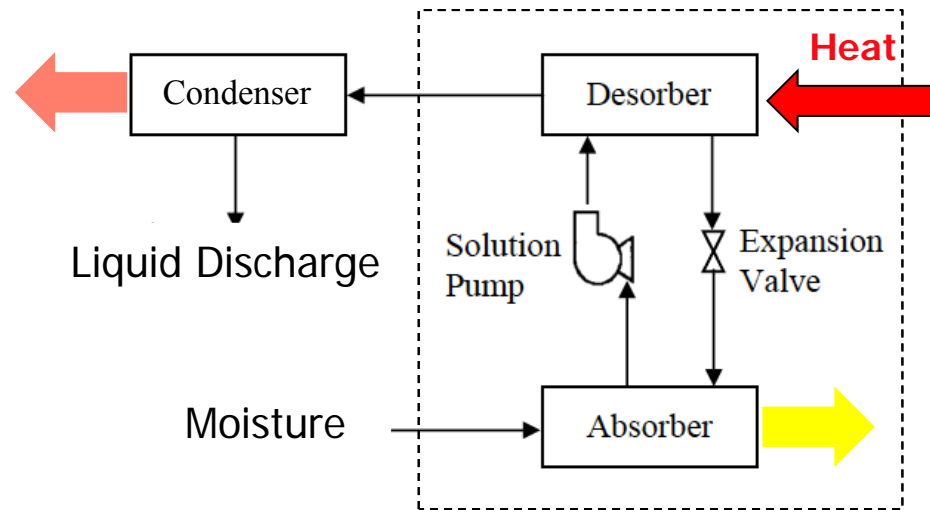
Research and Development Roadmap for Water Heating Technologies, Navigant, 2011

Operation Principle of an Absorption Cycle

Vapor compression cycle

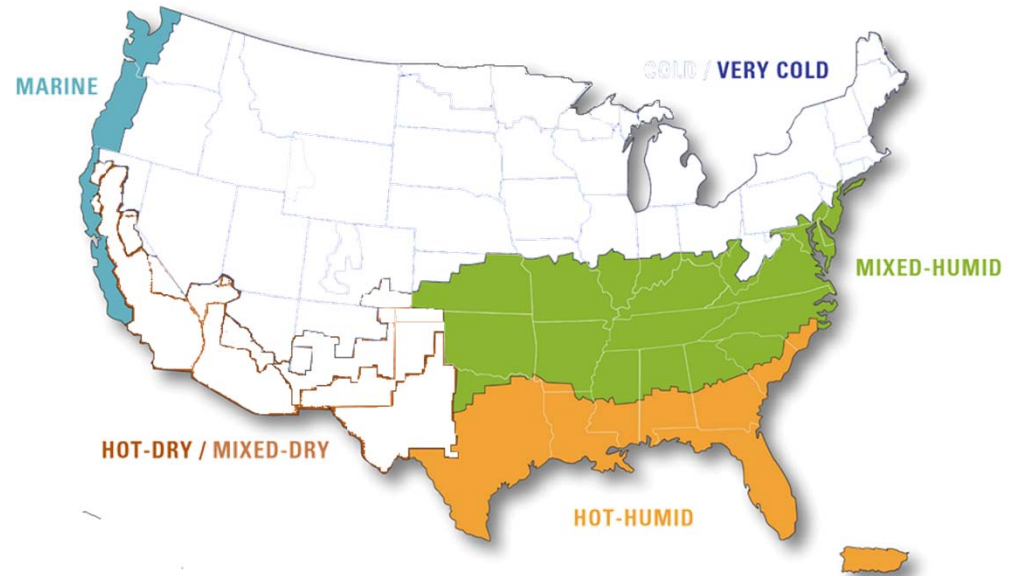


Open absorption system



Potential Application of Open System

- An open cycle can be substantially cheaper than a closed cycle
- Applicable to 3 zones, encompassing 54% of US homes



Environment	Ambient RH and Temperature	Thermal COP	Ambient Dew Point
Cold humid basement	6 °C, 80% RH	1.54	2.82
Humid open space	35 °C, 70% RH	1.72	28.7
Air-conditioned closed space	23 °C, 50% RH	1.63	12.06

Applicable in Buildings with Fresh Air Requirement

- Latent heat (i.e. heat of moisture) is the primary air ventilation load for much of the US (east, south, north, mid-west, north-west, and Islands)

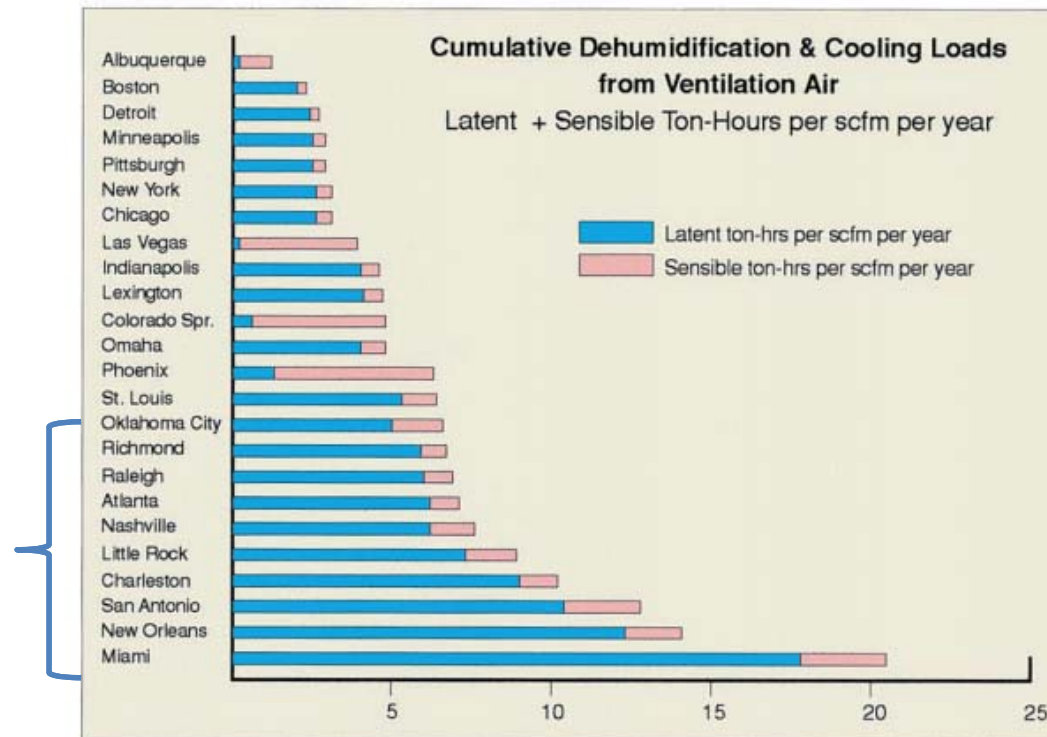
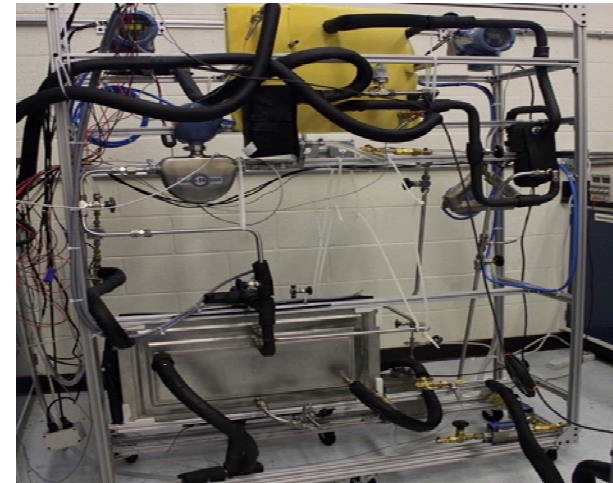
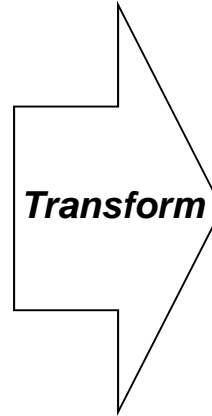
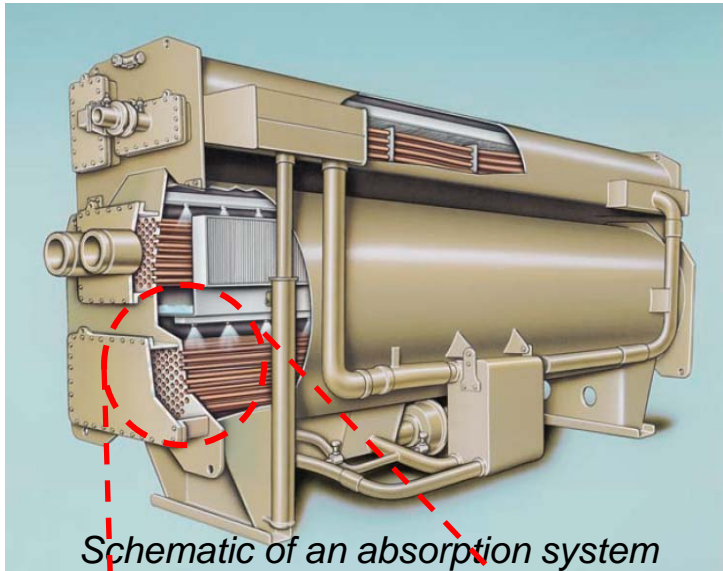


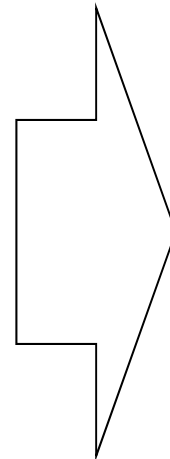
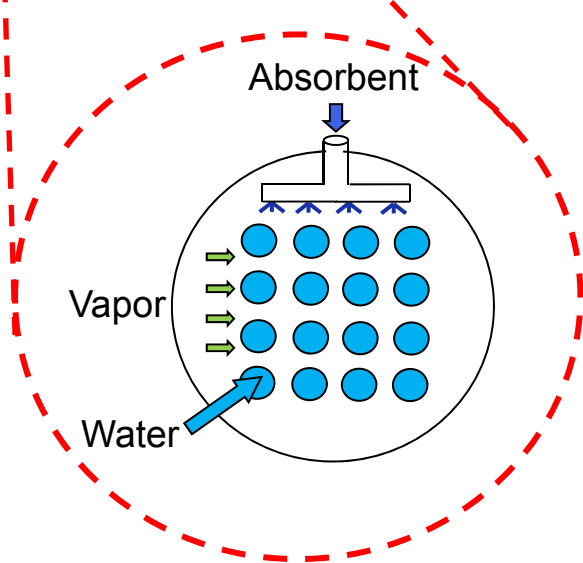
Fig. 2: Cumulative dehumidification and cooling loads from ventilation air for selected locations in the United States.

Benefits of a membrane-based absorption cycle

Membrane-based Closed Absorption System



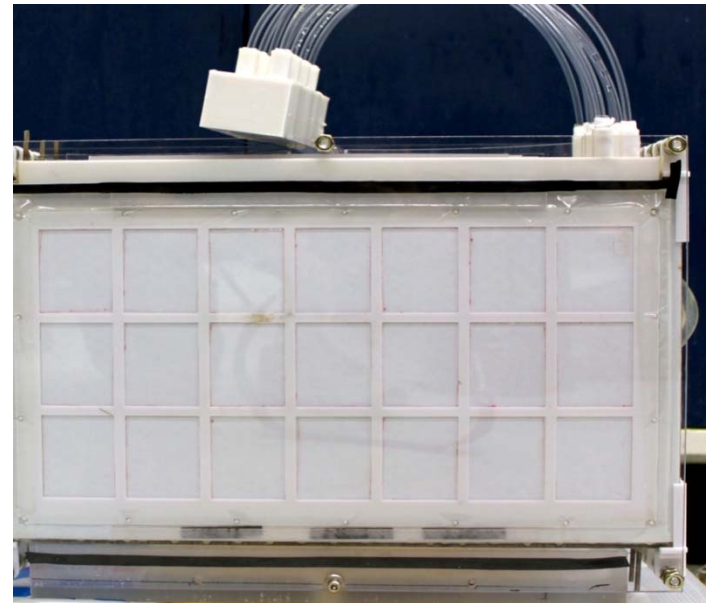
Compact absorption system



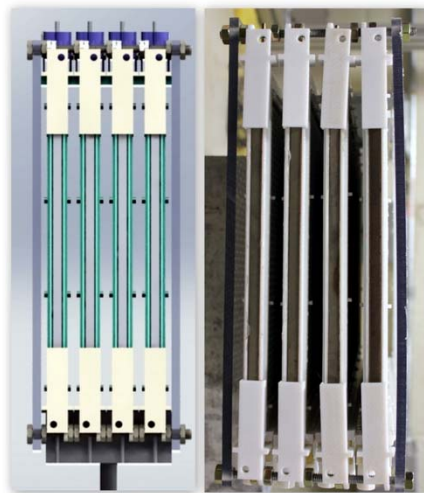
Membrane-based Open Absorption System



3D model of the absorber

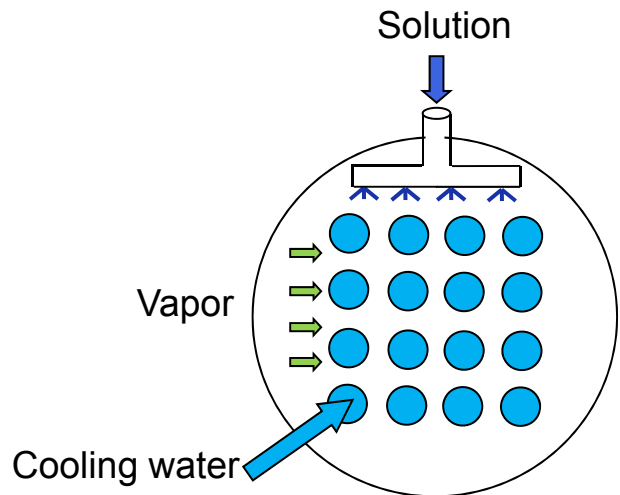


Fabricated absorber



Science of membrane-based absorption process

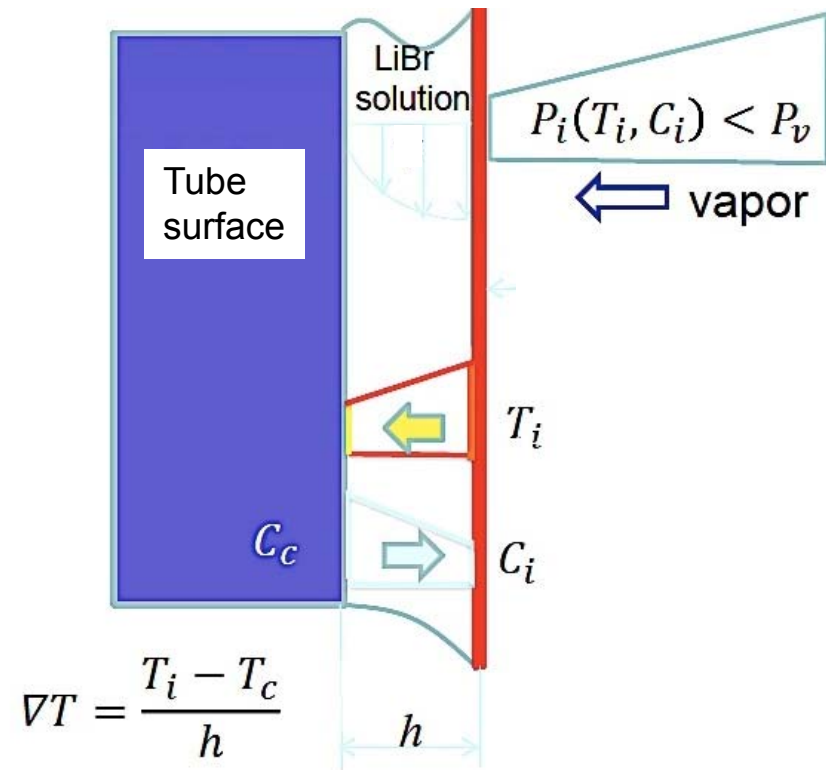
Absorber Heat Exchanger



Control factors in absorption rate:

Film thickness: h ; solution velocity v

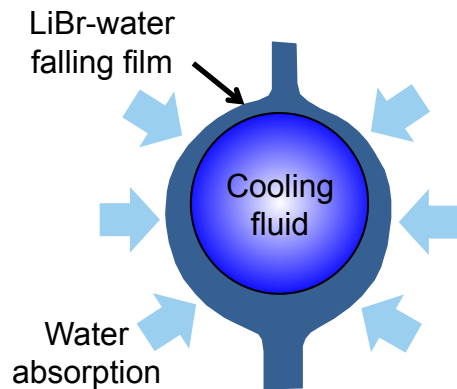
Cooling water temperature T_c



$$\nabla T = \frac{T_i - T_c}{h}$$

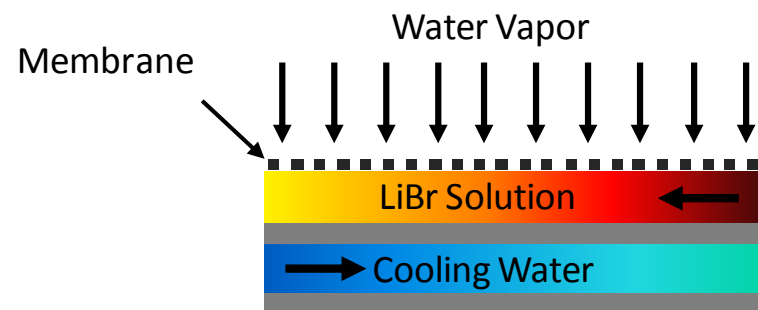
Membrane-based Absorber vs. Current Absorbers: Fundamental Physics

Conventional



- Hydrodynamics of the falling film over the tubes dictates the film thickness
 - Film thickness is not optimal for maximum absorption
 - Flow velocity is coupled with the film thickness

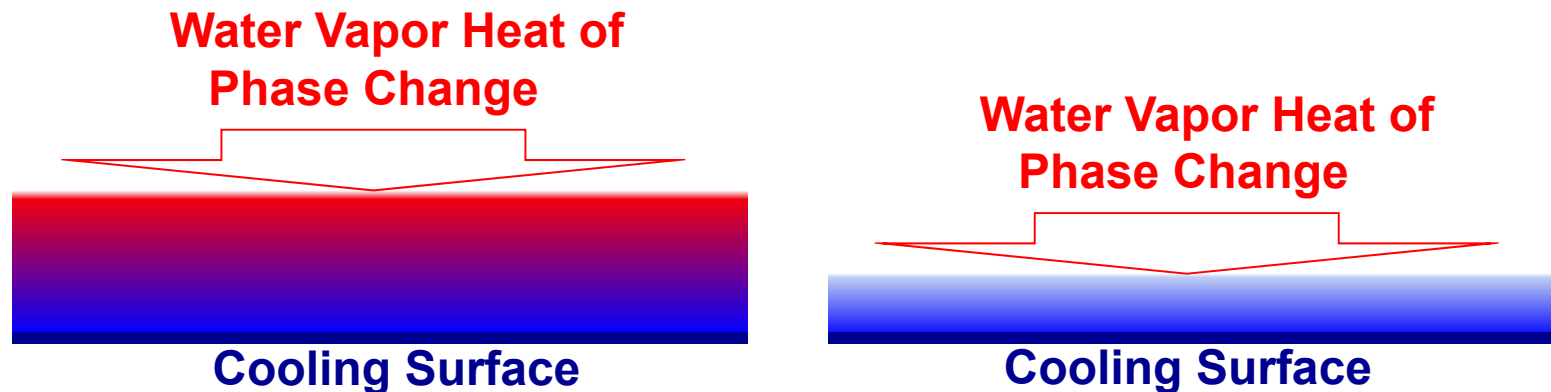
Membrane-based



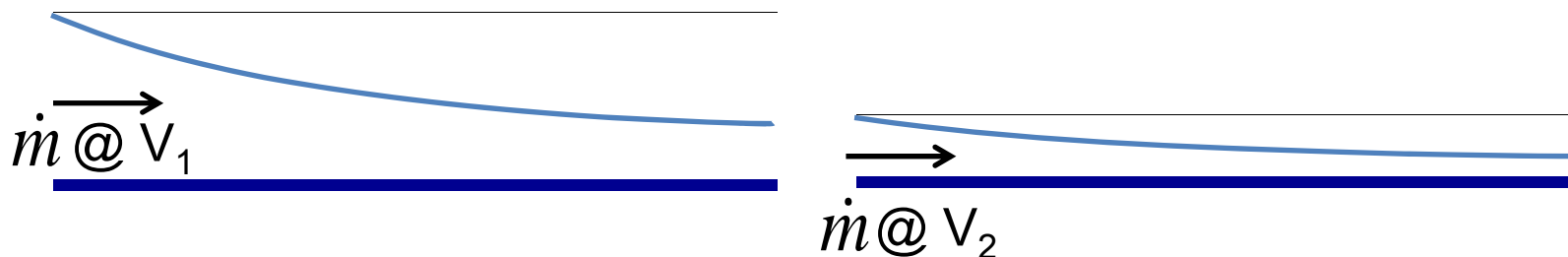
- Utilize thin absorbent films constrained by highly permeable membranes
 - Enables independent control over the film thickness and velocity
 - Enables fabrication of compact plate-and-frame absorbers

Effect of Film Thickness and Velocity on Absorption Rate

- Better cooling of the solution/vapor interface

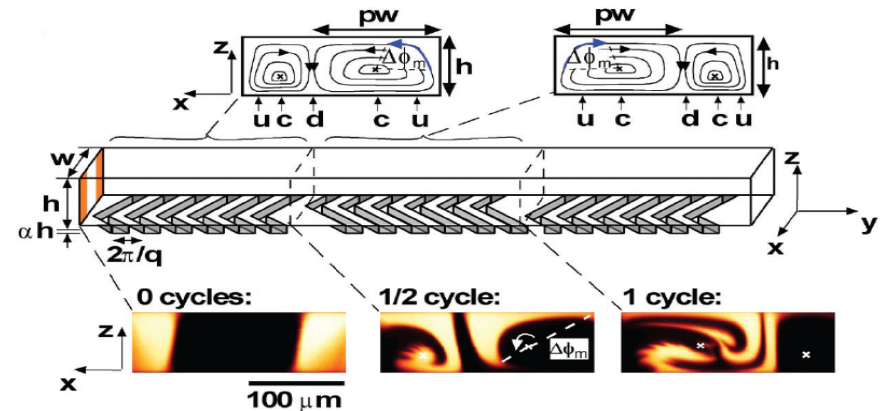


- Reduced mass transfer resistance

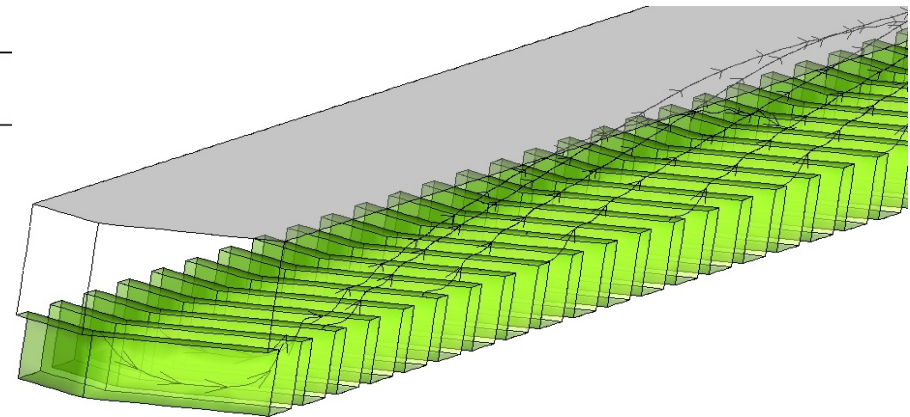
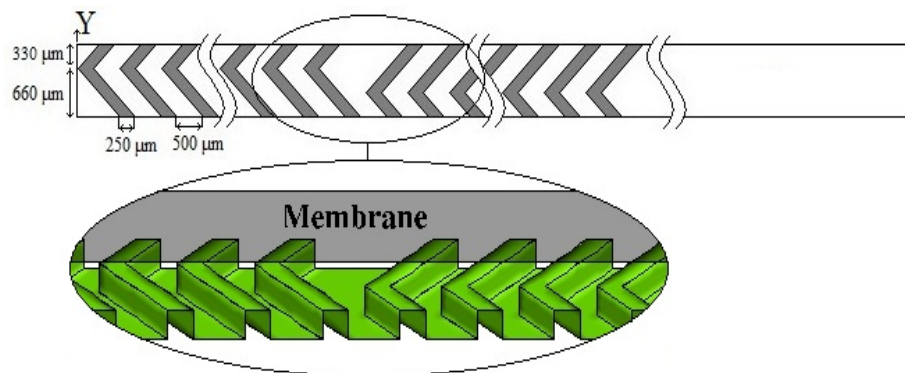


2nd Generation Absorber

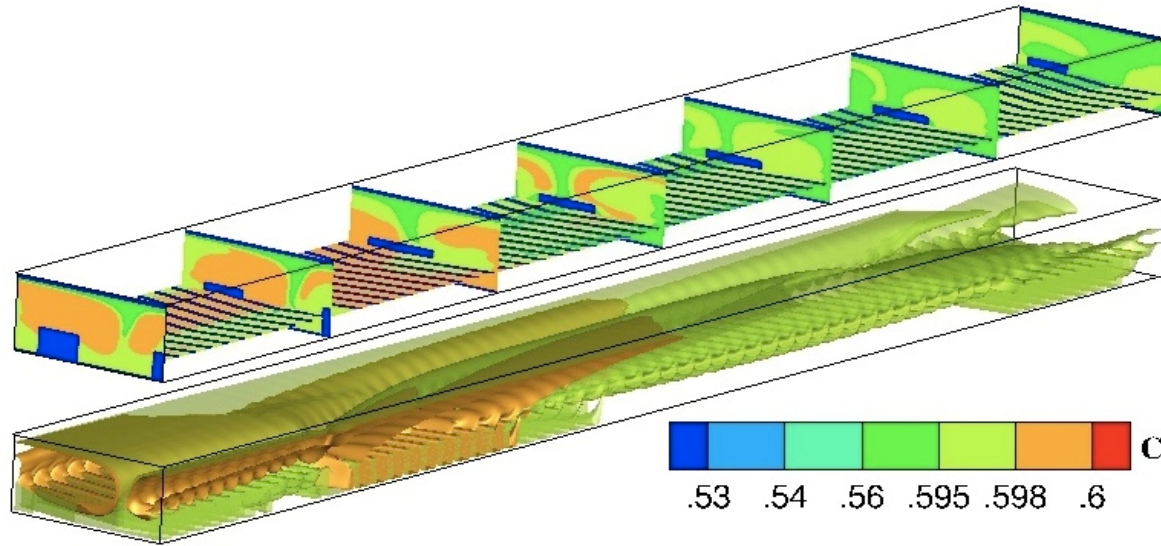
- Use a thick liquid layer to reduce the pressure drop
- Chaotic mixing of the solution flow
 - Overcome diffusion limitations
- Using surface microstructures to generate vortices



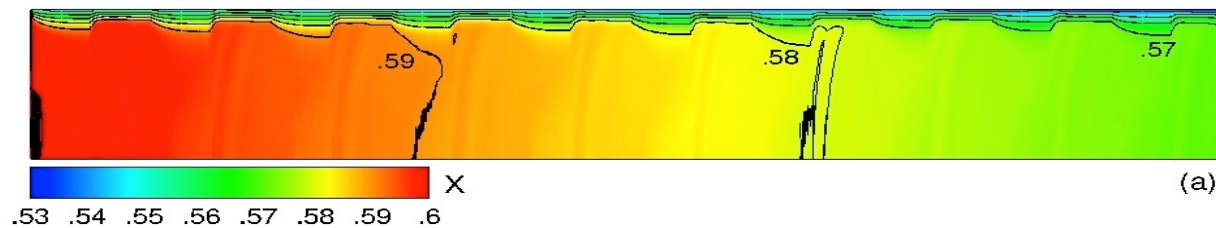
A. D. Stroock et al., Science, 2002



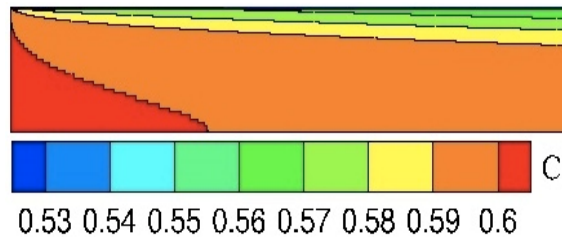
2nd Generation Absorber



With mixing

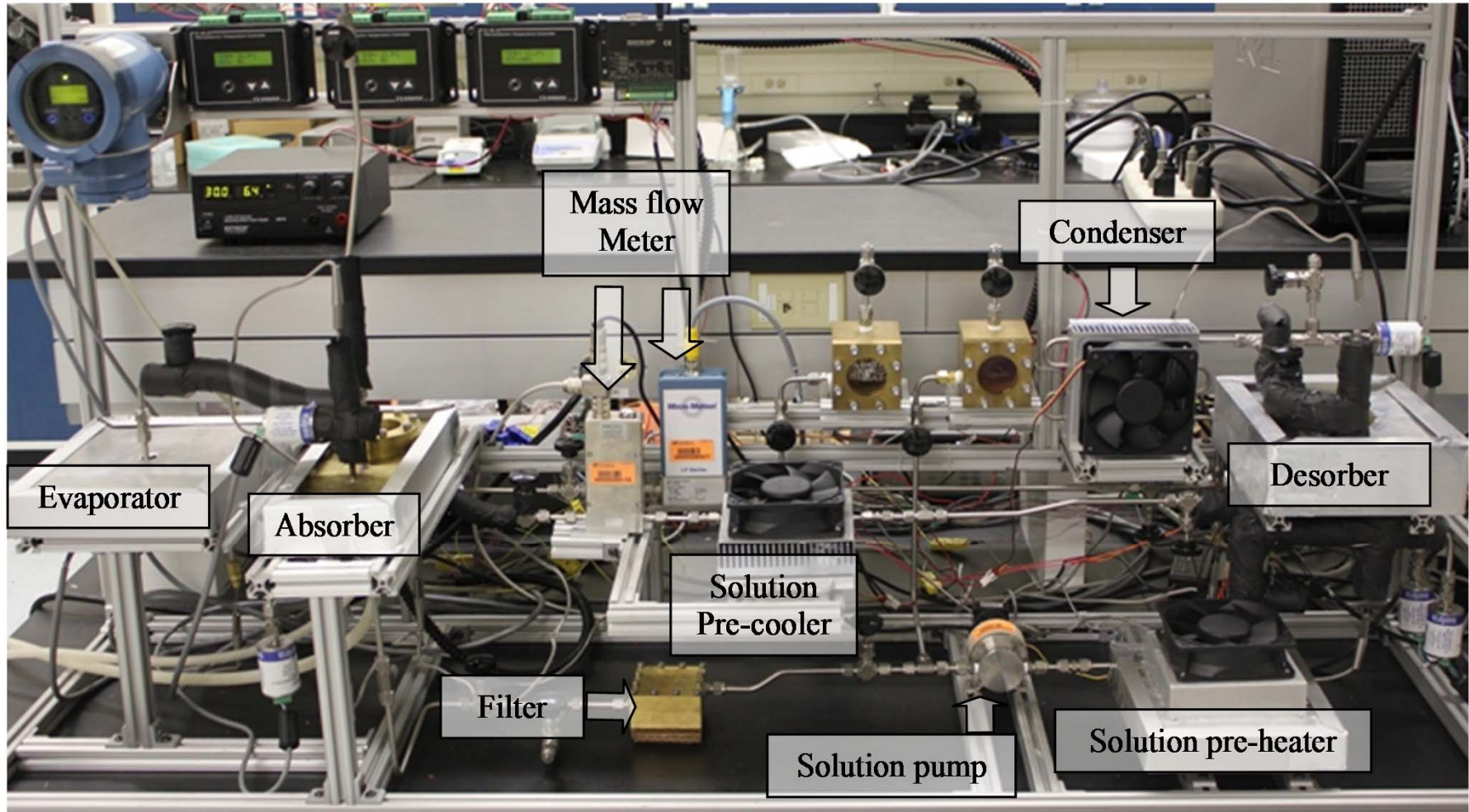


Without mixing

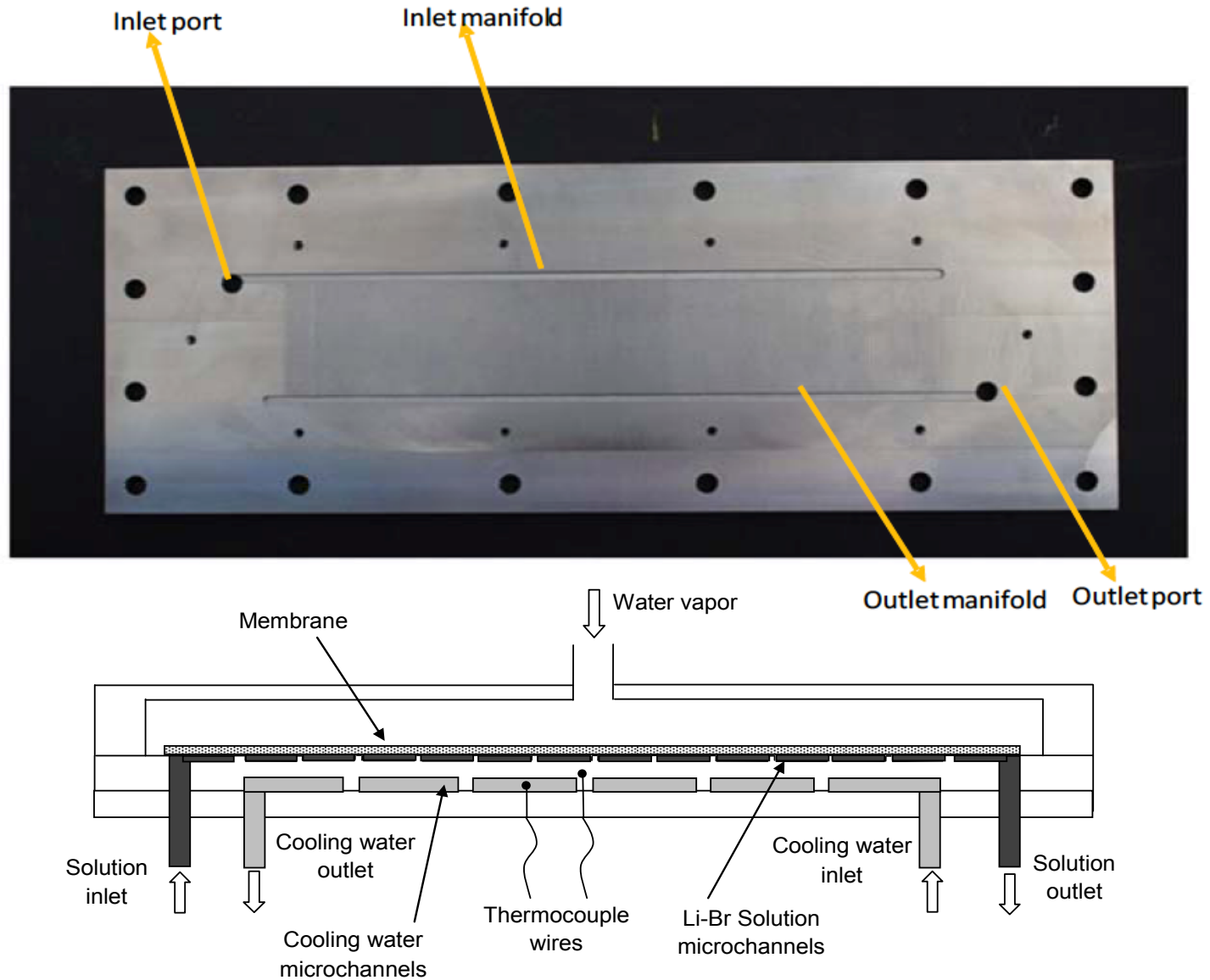


Scaled by a factor of 100 in the x-direction

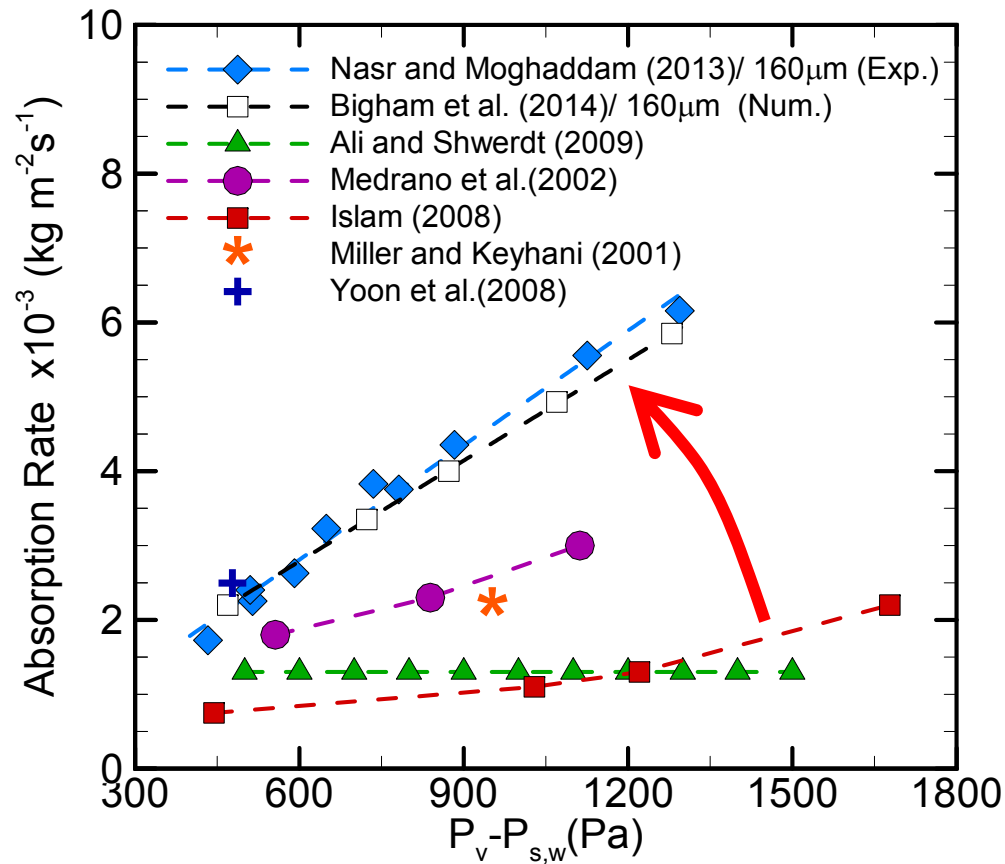
Experimental Equipment



1st Generation Absorber

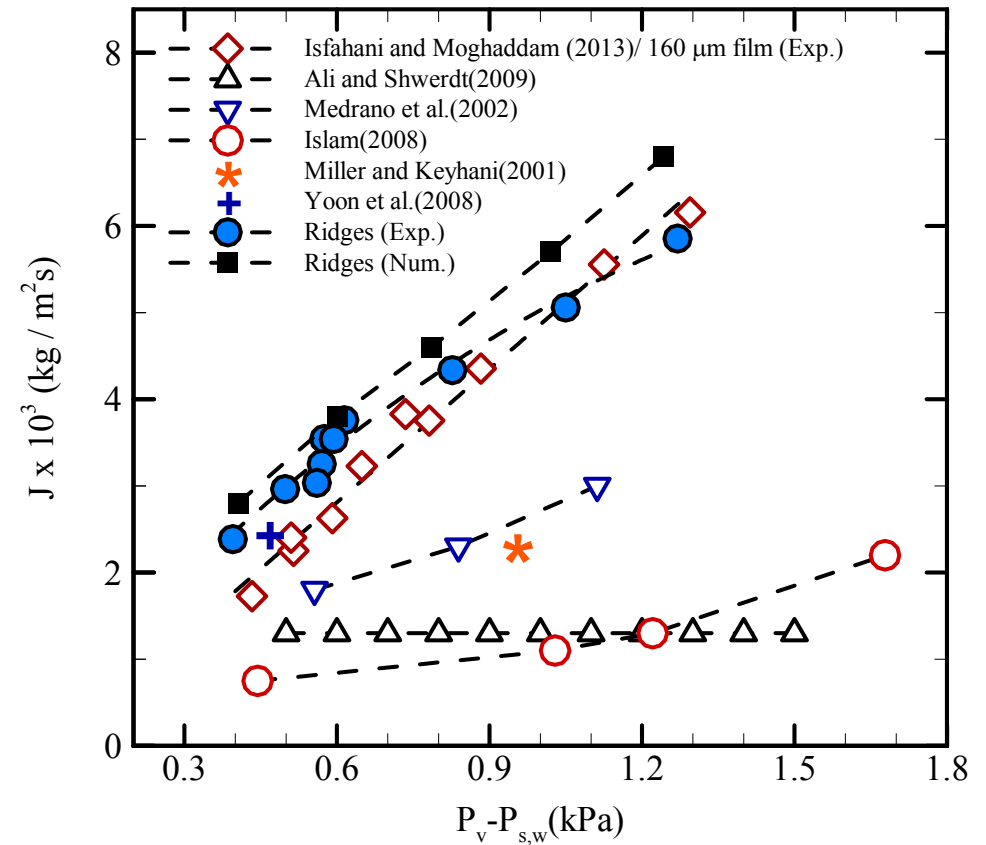
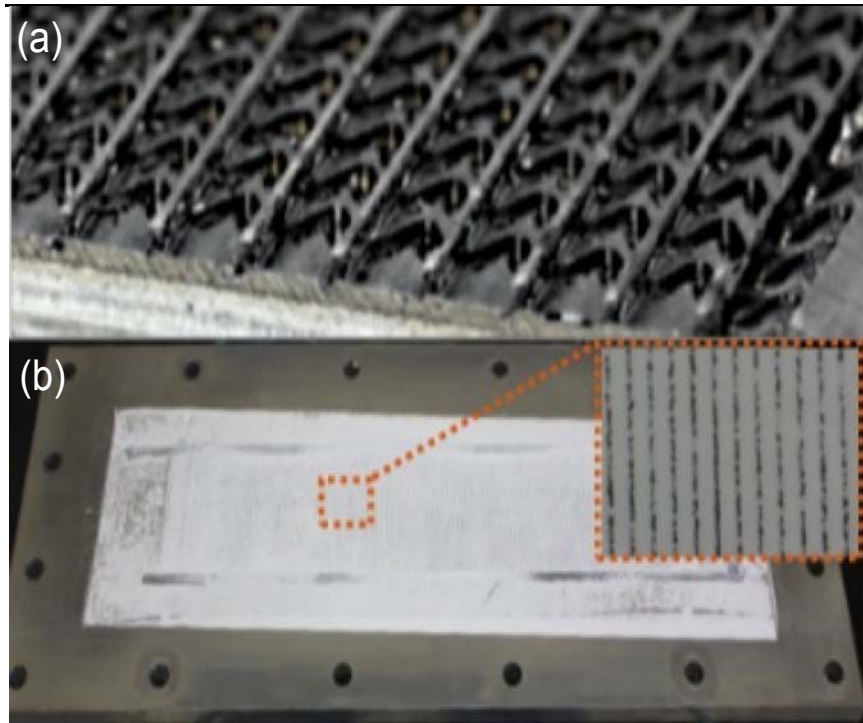


1st Generation Absorber

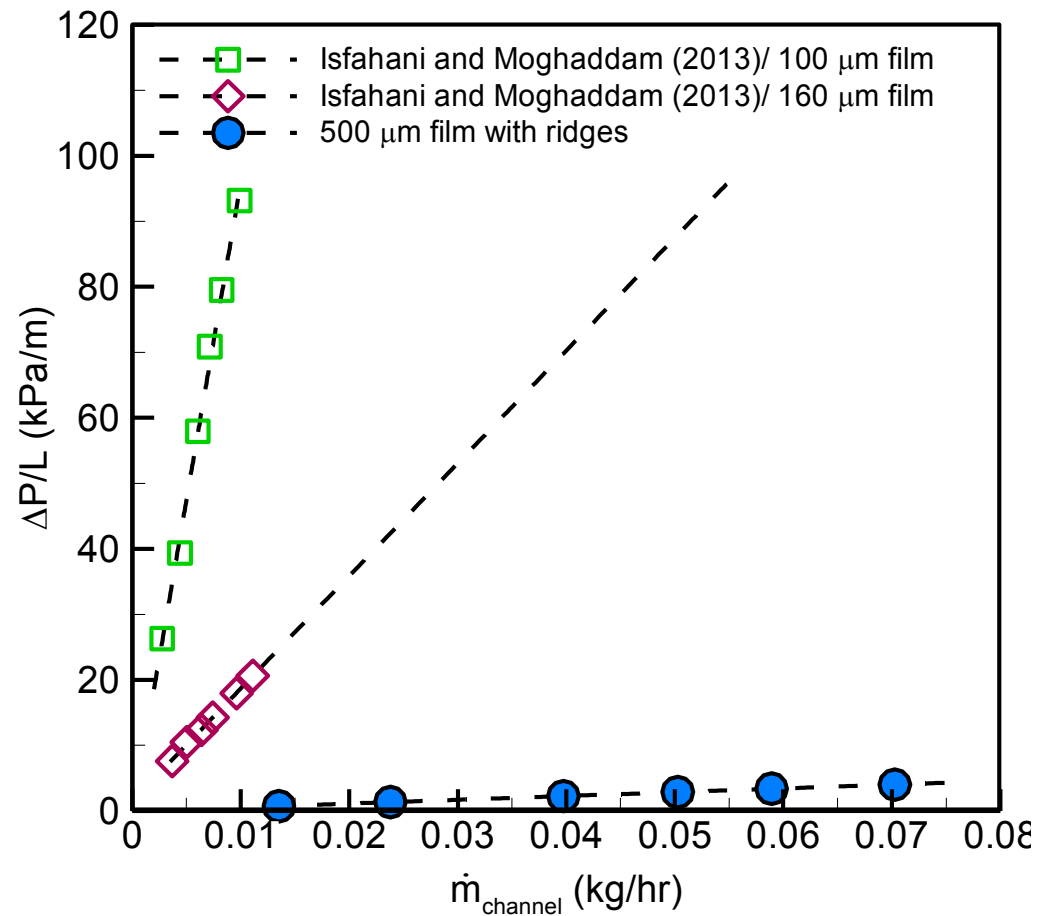


Nasr and Moghaddam, Int. J. Heat Mass Transfer, 2013

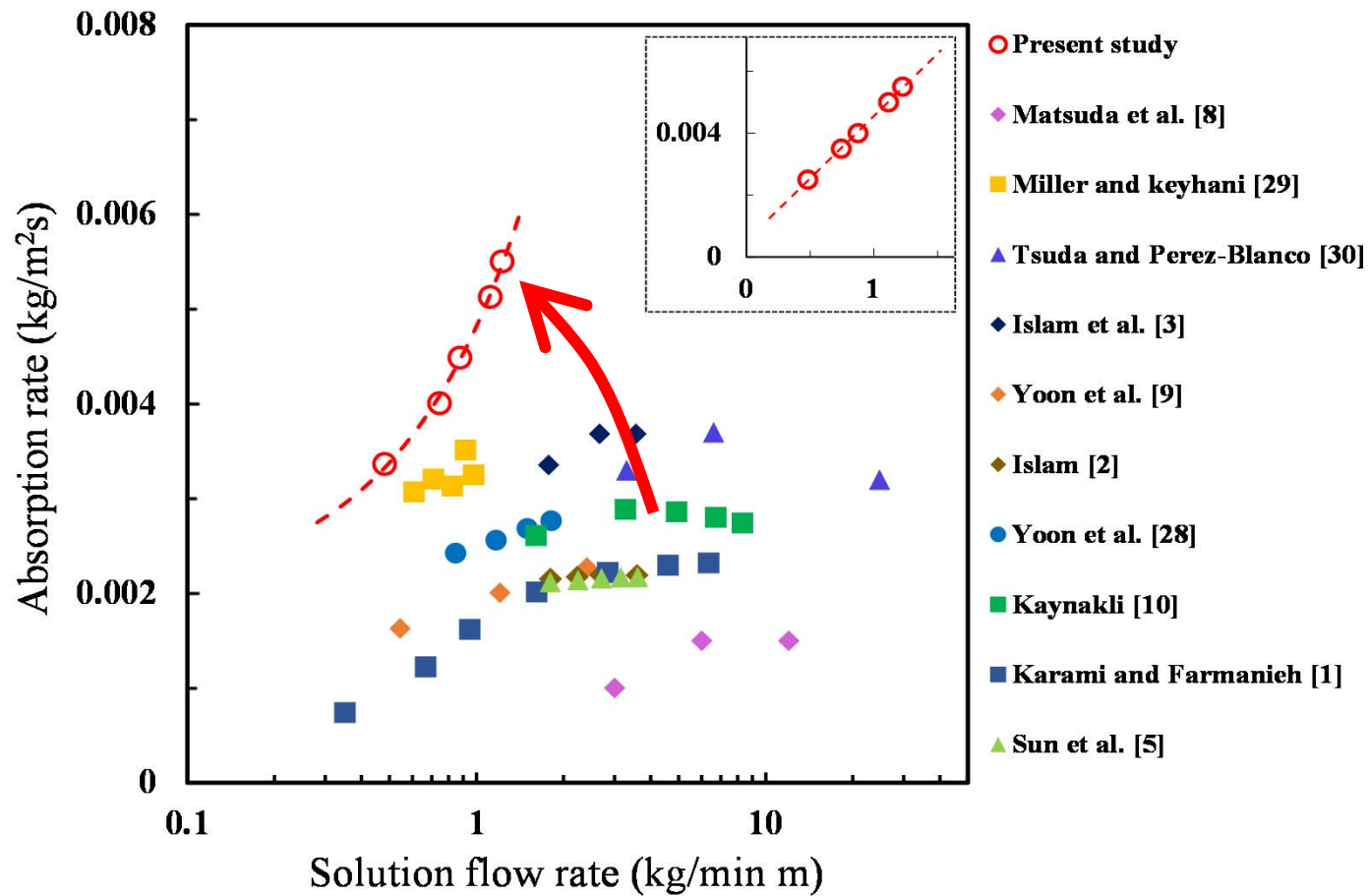
2nd Generation Absorber



Comparison of 1st and 2nd Generations Pressure Drop

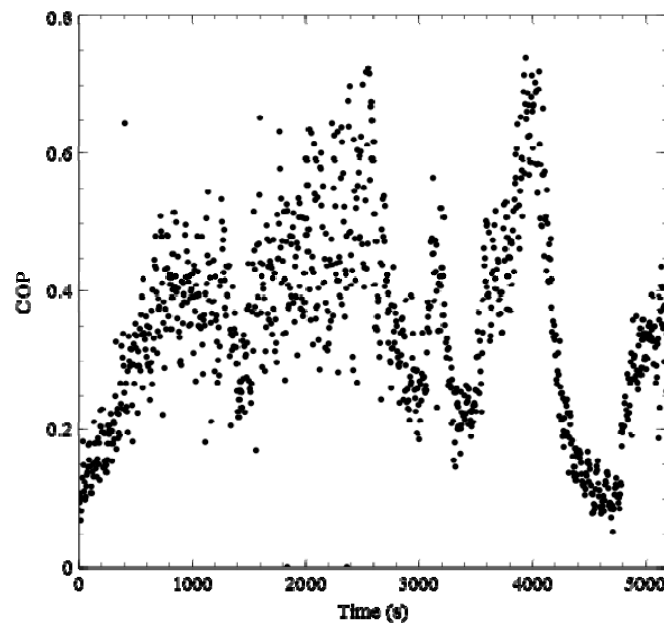
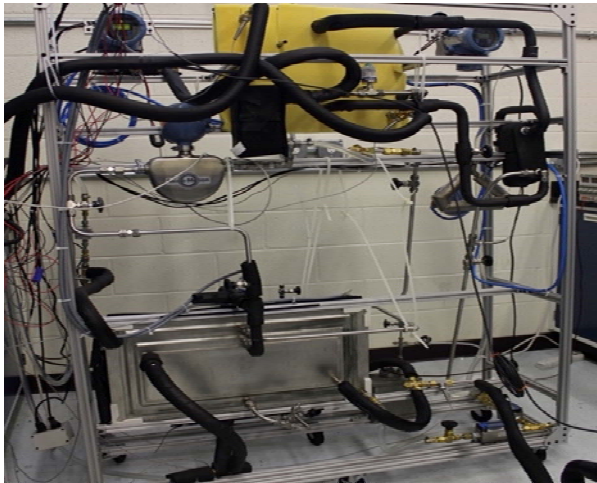


3rd Generation Absorber



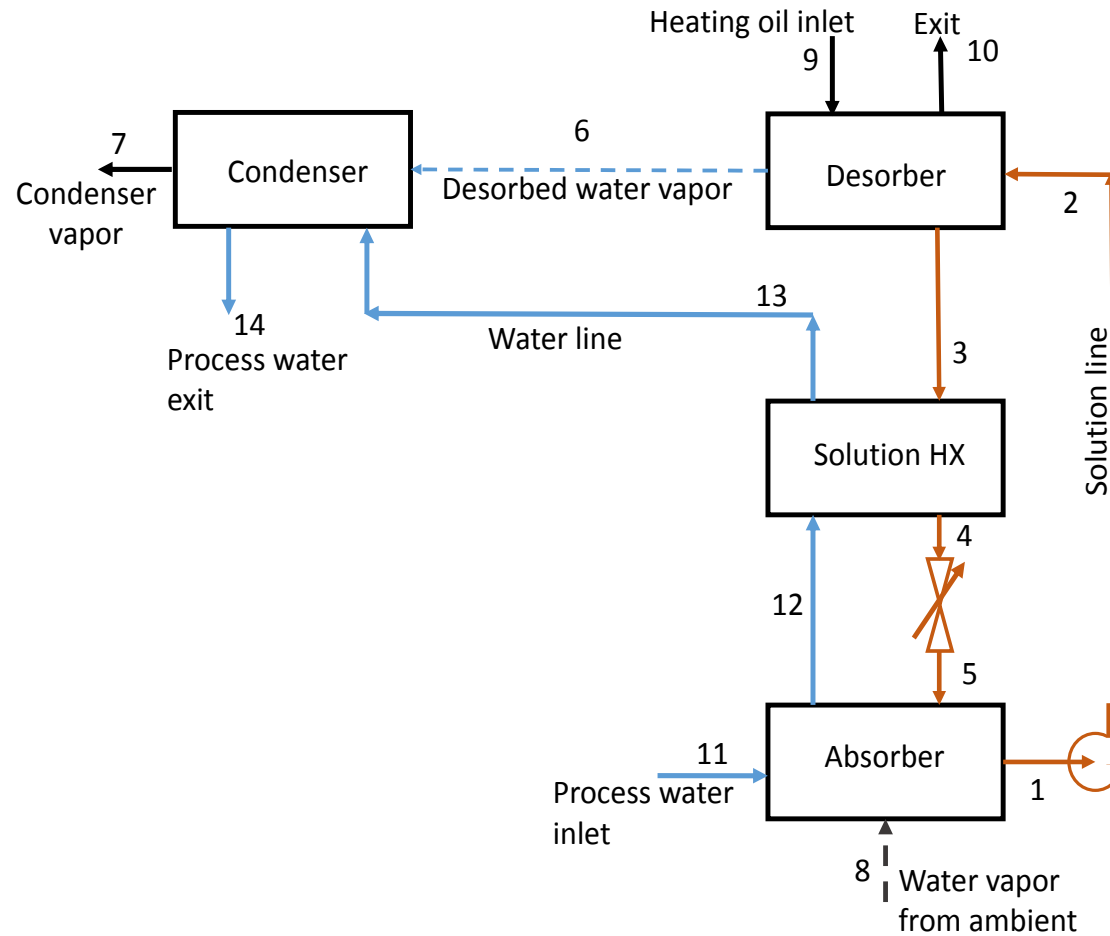
Systems level testing

1st Generation Closed System

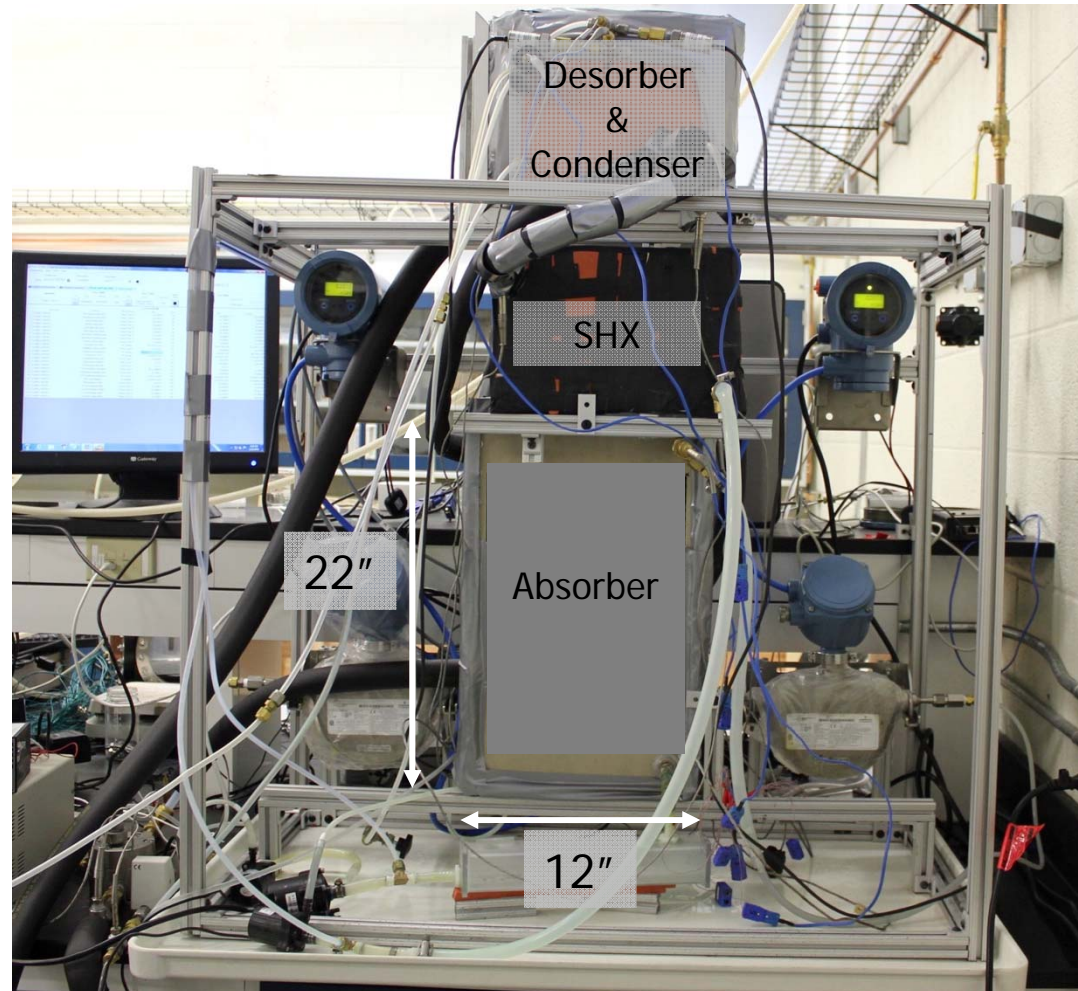


- Test conditions:
 - $T_{\text{supl-evap}} = 12^{\circ} \text{C}$
 - $T_{\text{supl-abs}} = 25^{\circ} \text{C}$
 - $\text{COP}_{\text{heating}} = 1.7$
- Highly unstable
- Identified the source of instability
- 2nd generation has been fabricated
- Tests on the new system will be conducted soon

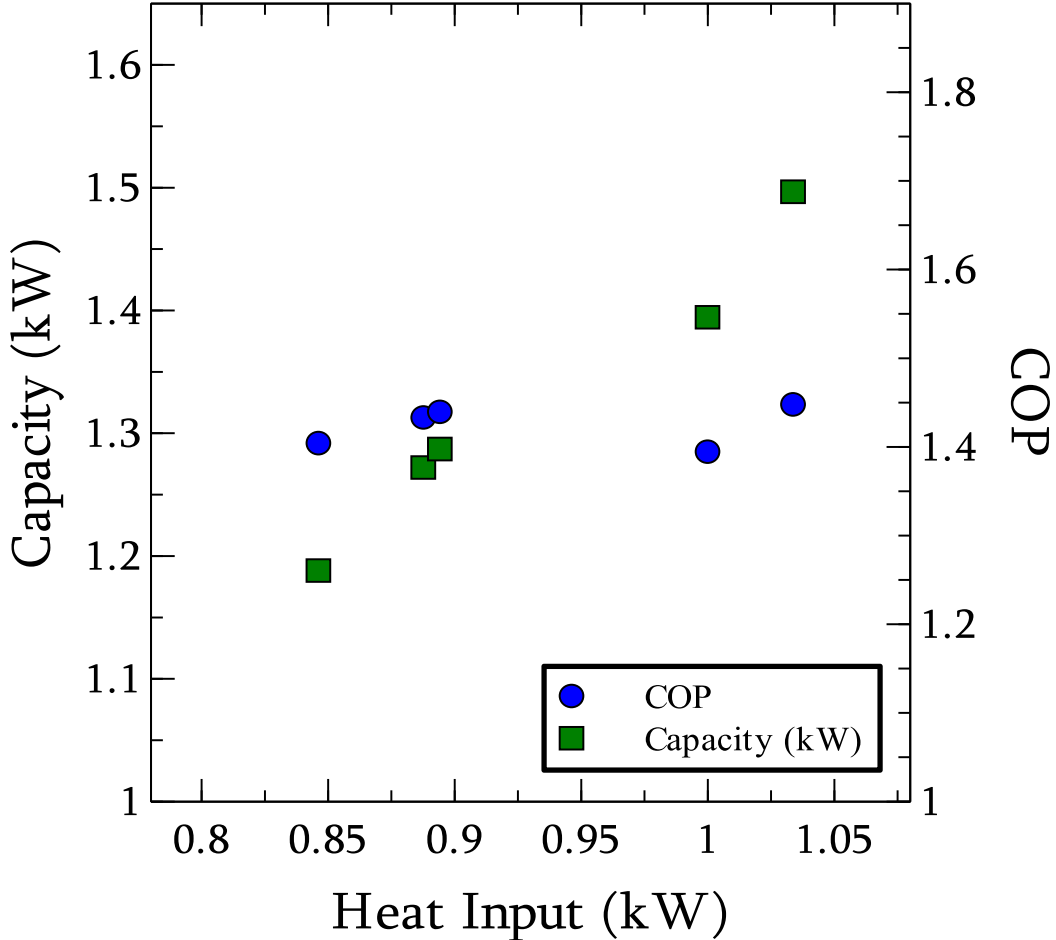
1st Generation Open Architecture Water Heater



1st Generation Open Architecture Water Heater

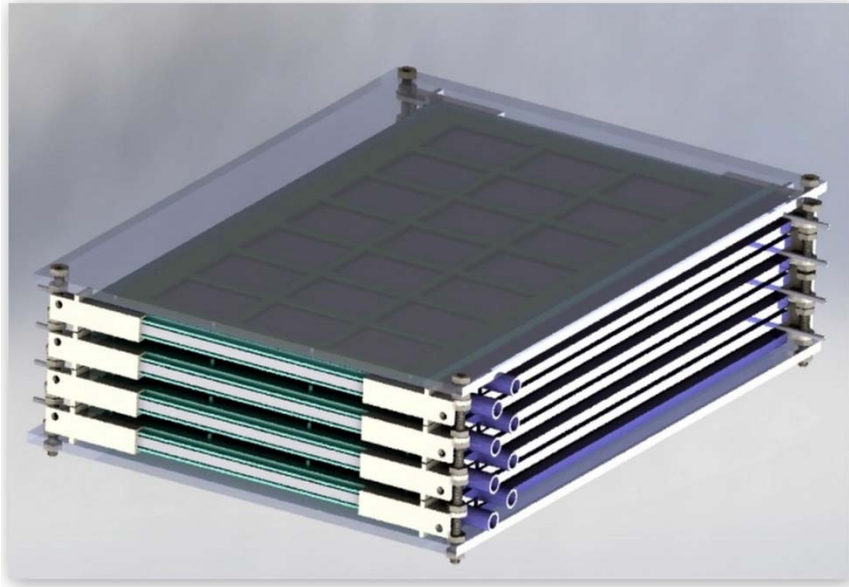


Performance Data of Open Architecture Water Heater

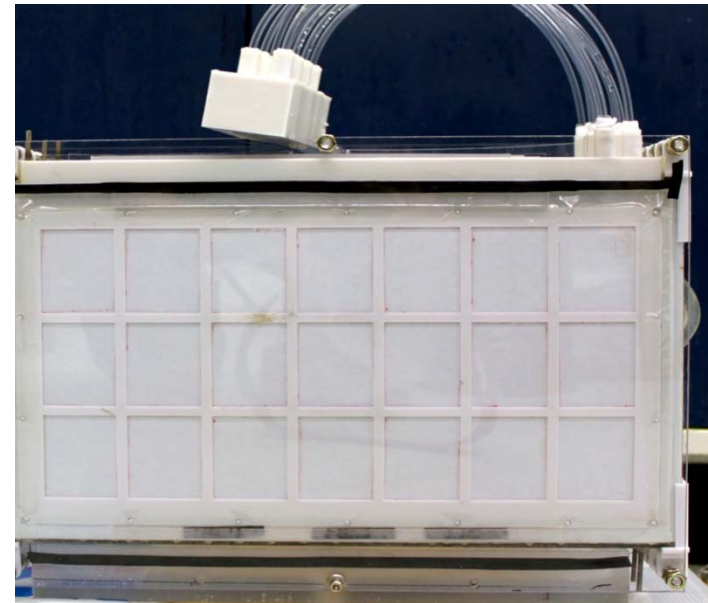


Performance of a LiBr system at $\sim 20-23^{\circ}\text{C}$ and 60-65% RH

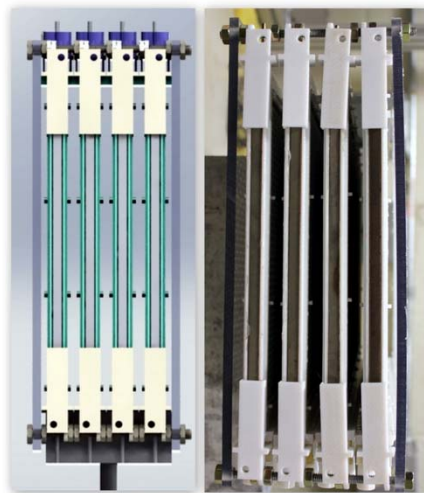
2nd Generation Open Architecture Water Heater



3D model

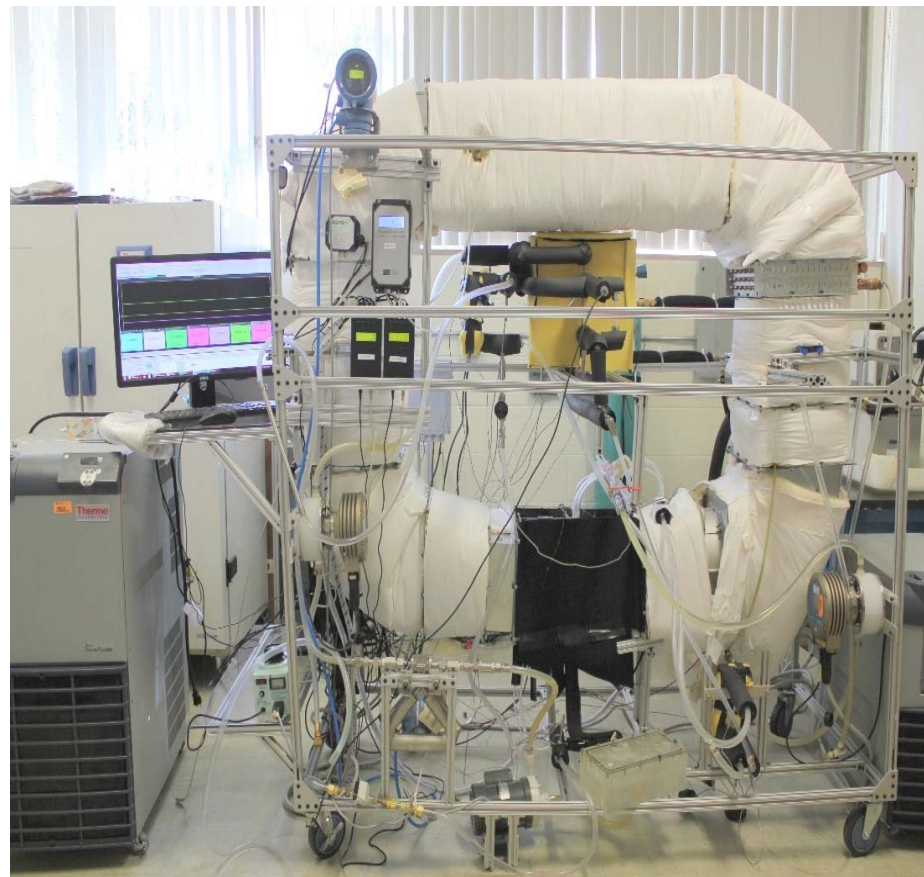


Fabricated device



Experimental Loop

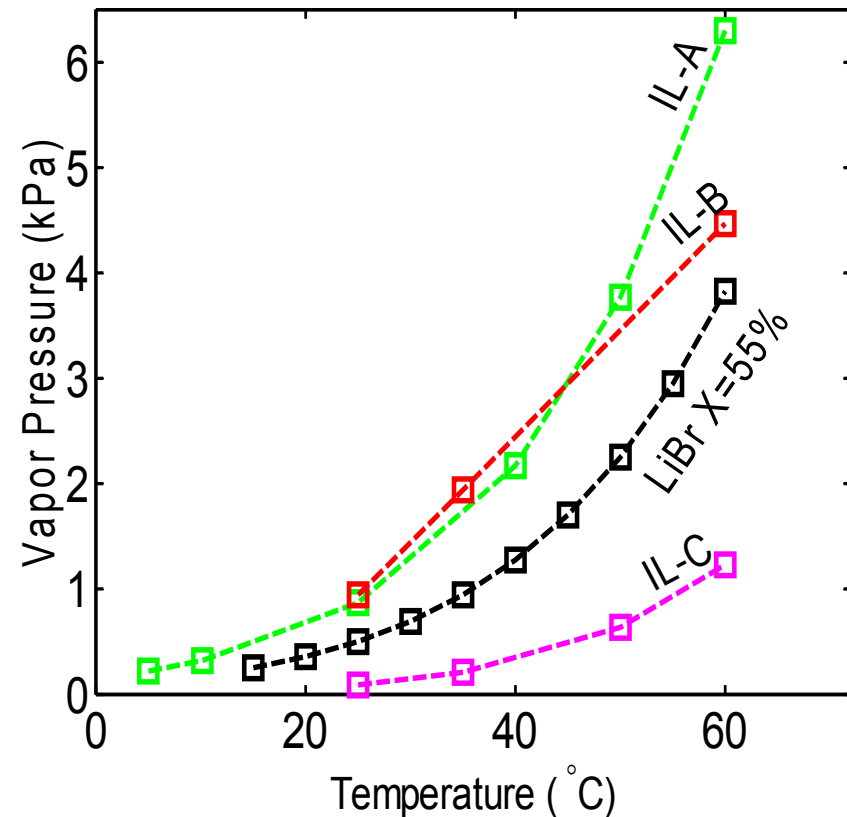
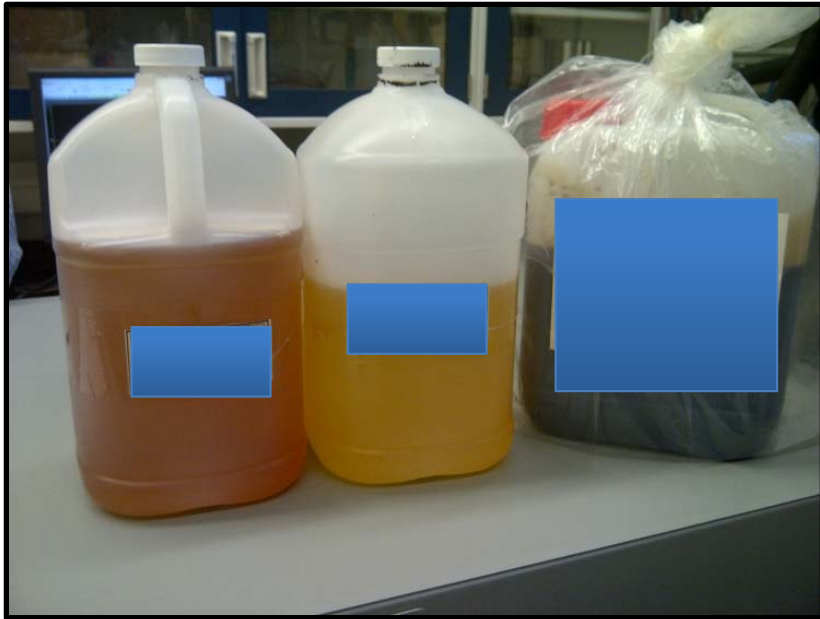
- Fully instrumented air conditioning system
- With control on temperature and humidity



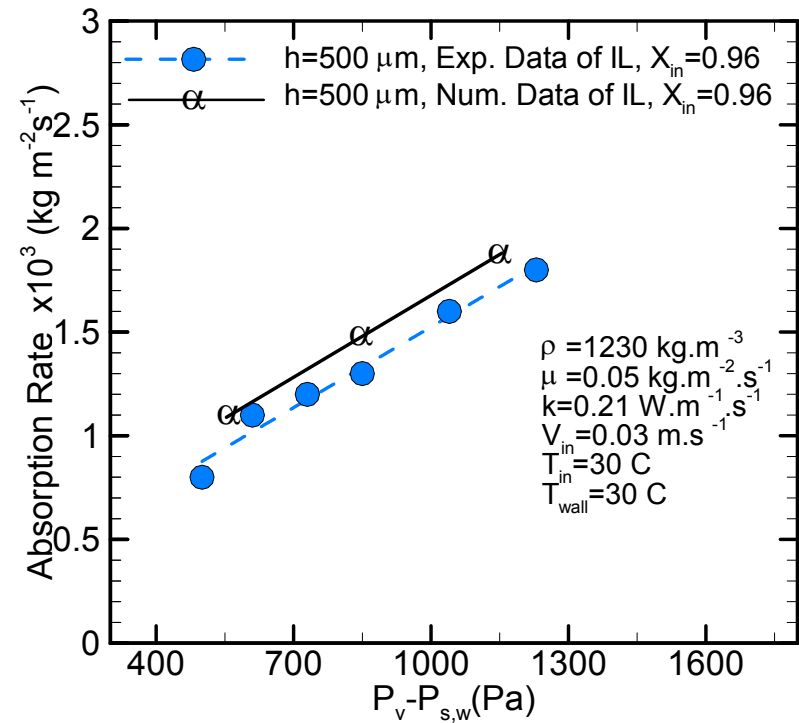
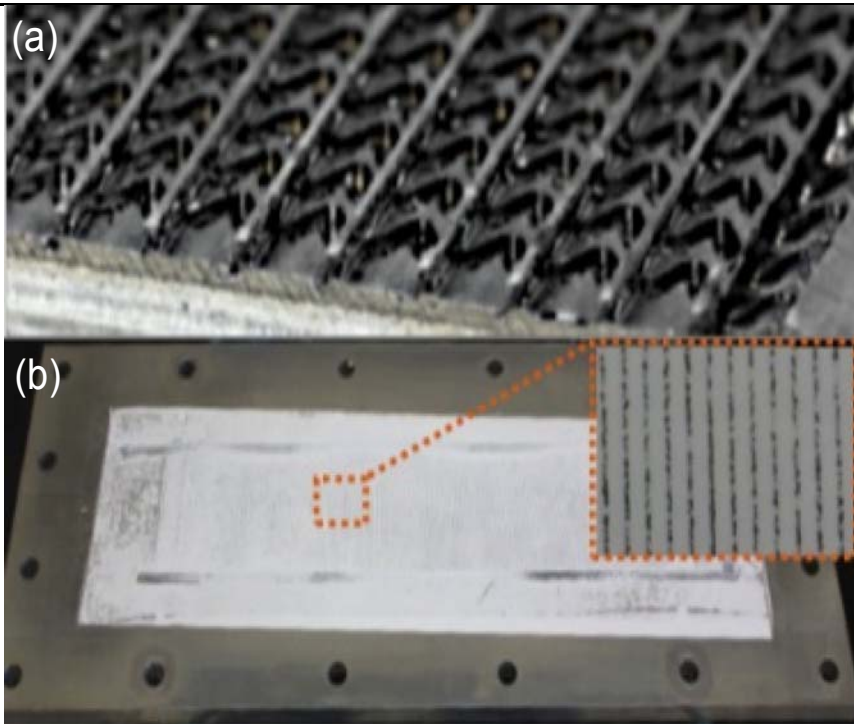
Ionic liquids

New Opportunities with Ionic Liquids (ILs)

- Crystallization issue is addressed
- Less corrosive than the LiBr solution
- Low vapor pressure at high absorber temperature
- Environment friendly (green liquids!)



Preliminary Experimental Results (closed system)



Momentum, Energy and Concentration:

$$\rho u_j u_{i,j} = -p_i + \mu u_{i,jj}$$

$$u_j T_{,j} = \alpha T_{,jj}$$

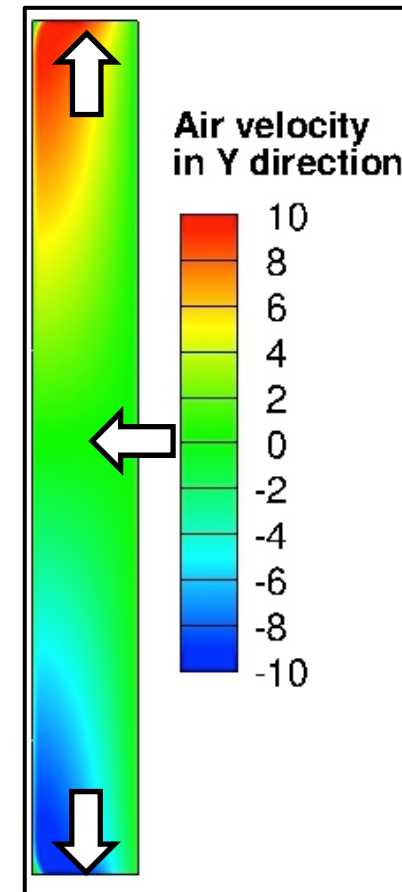
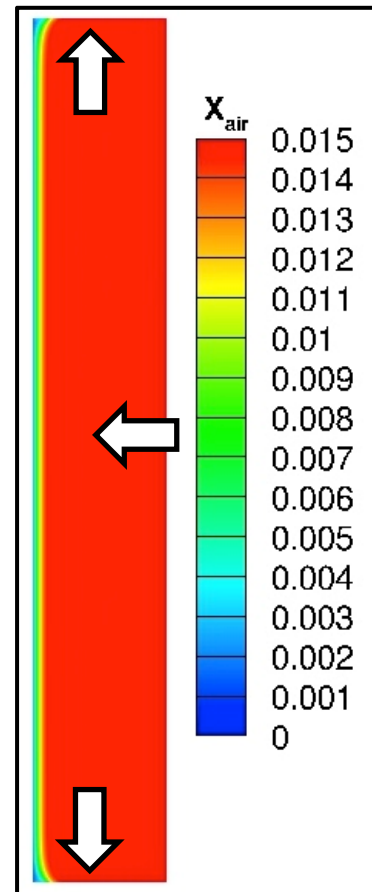
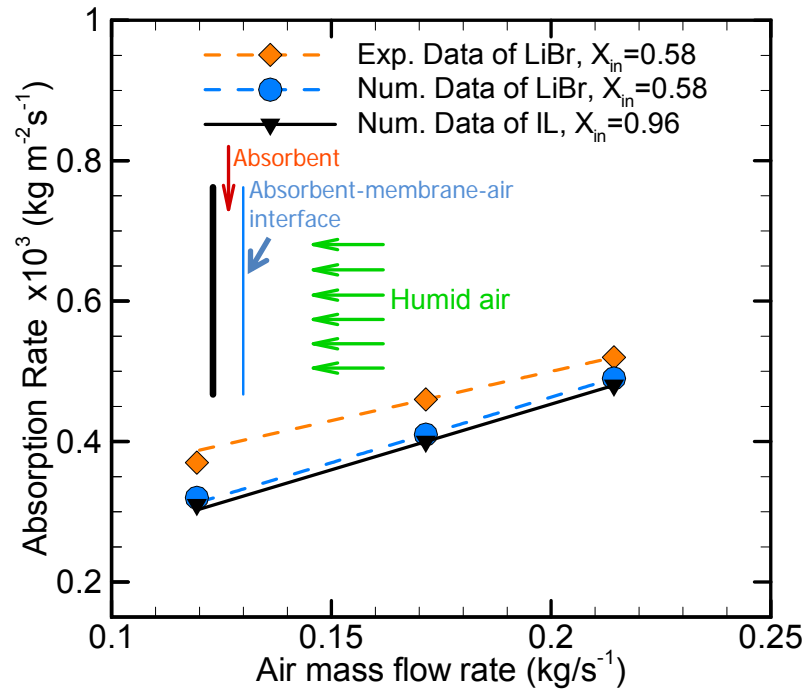
$$u_j X_{,j} = D X_{,jj}$$

Dusty-Gas model to calculate the vapor flow rate through the membrane pores:

$$J = k_m (P_v - P_{s,w})$$

$$k_m = -\left(M / \delta_m\right) \left[D_e^k / (RT) + PB_0 / (RT \mu) \right]$$

Numerical Analysis



Conclusions

- Absorption systems can be transformed into compact, light, and inexpensive configurations
 - 2nd generation closed LiBr system is fabricated and will be tested soon
 - 2nd generation open system with an ionic liquid is fabricated and currently being tested

- Ionic liquids enable overcoming the traditional operation limits of absorption cycles
 - Avoid crystallization
 - Robust and low cost system
 - High water output temperature

Acknowledgements



Thank you

Publications and Patents

Publications

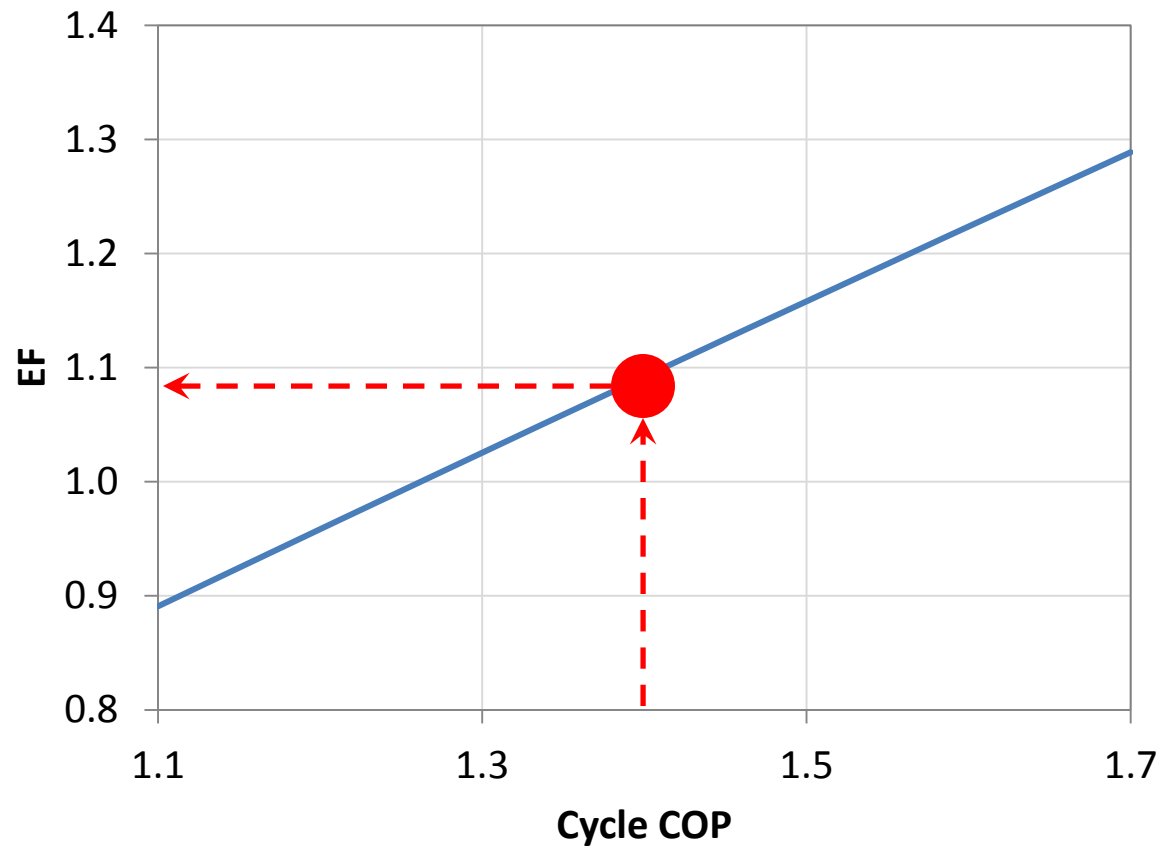
- S. Bigham, R. Nasr Isfahani, and S. Moghaddam, "Direct Molecular Diffusion and Micro-mixing for Rapid Dewatering of LiBr Solution," *Applied Thermal Engineering*, vol. 64, pp. 371-375, 2014.
- R. Nasr Isfahani, A. Fazeli, S. Bigham, and S. Moghaddam, "Physics of Lithium Bromide (LiBr) Solution Dewatering Through Vapor Venting Membranes," *International Journal of Multiphase Flow*, vol. 58, pp. 27-38, 2014.
- S. Bigham, D. Yu, D. Chugh, and S. Moghaddam, "Moving Beyond the Limits of Mass Transport in Liquid Absorbent Microfilms through the Implementation of Surface-Induced Vortices," *Energy*, vol. 65, pp. 621-630, 2014.
- R. Nasr Isfahani, K. Sampath, and S. Moghaddam, "Nanofibrous Membrane-based Absorption Refrigeration System," *International Journal of Refrigeration*, vol. 36, pp. 2297-2307, 2013.
- R. Nasr Isfahani and S. Moghaddam, "Absorption Characteristics of Lithium Bromide (LiBr) Solution Constrained by Superhydrophobic Nanofibrous Structures," *International Journal of Heat and Mass Transfer*, vol. 63 (5-6), pp. 82-90, 2013.
- D. Yu, J. Chung, and S. Moghaddam, "Parametric Study of Water Vapor Absorption into a Constrained Thin Film of Lithium Bromide Solution," *International Journal of Heat and Mass Transfer*, vol. 55 (21-22), pp. 5687-5695, 2012.

Patents

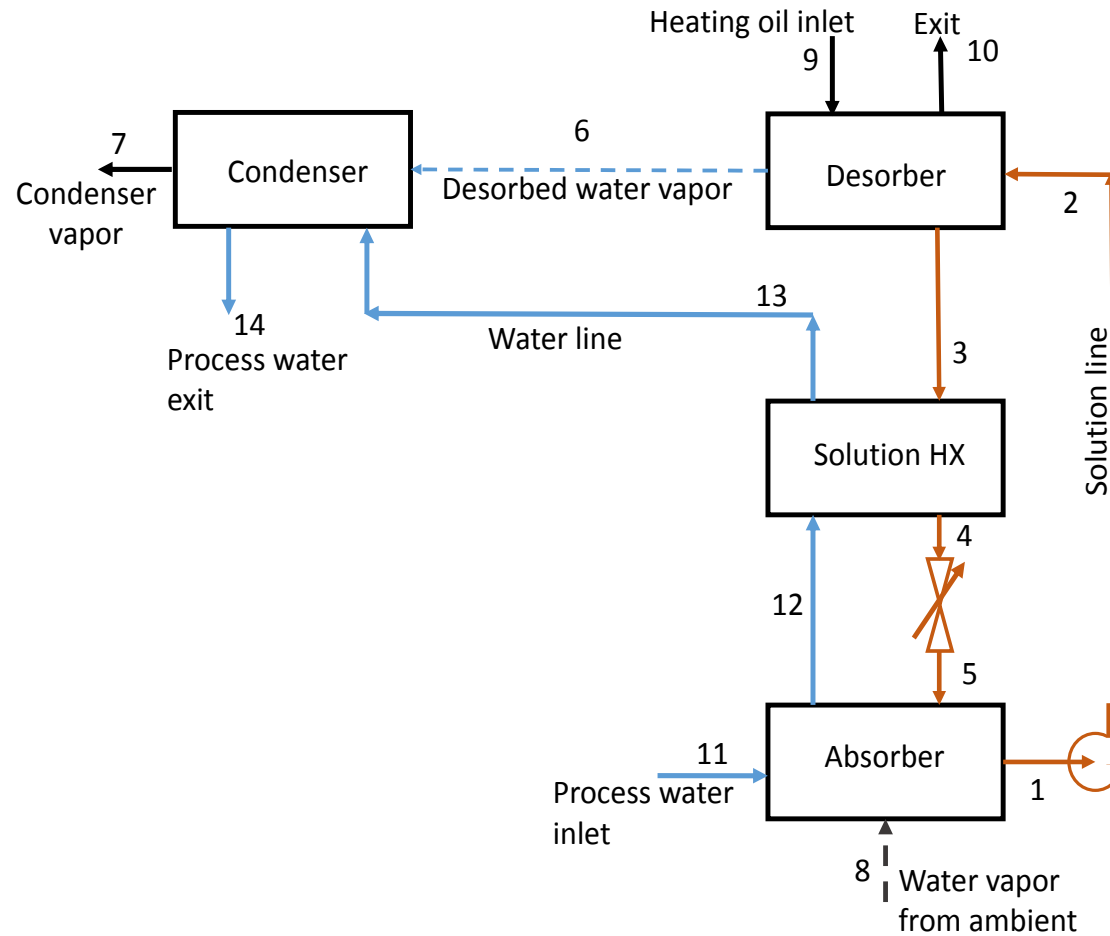
- S. Moghaddam, D. Chugh, R. Nasr Isfahani, S. Bigham, A. Fazeli, D. Yu, M. Mortazavi, and O. Abdelaziz, Open Absorption Cycle for Combined Dehumidification, Water Heating, and Evaporating Cooling, Patent Application UF-14820, 2013.
- S. Moghaddam and D. Chugh, Novel Architecture for Absorption-based Heaters, Patent Application UF-14697, 2013.
- S. Moghaddam, Thin Film-based Compact Absorption Cooling System, WO Patent 2,013,063,210, 2013.
- S. Moghaddam, D. Chugh, S. Bigham, 3D Microstructures for rapid Absorption and Desorption in Mechanically Constrained Liquid Absorbents, UF Patent#14936, 2013

Energy Factor (EF)

- Projected system EF (water heating) based on absorption cycle test results

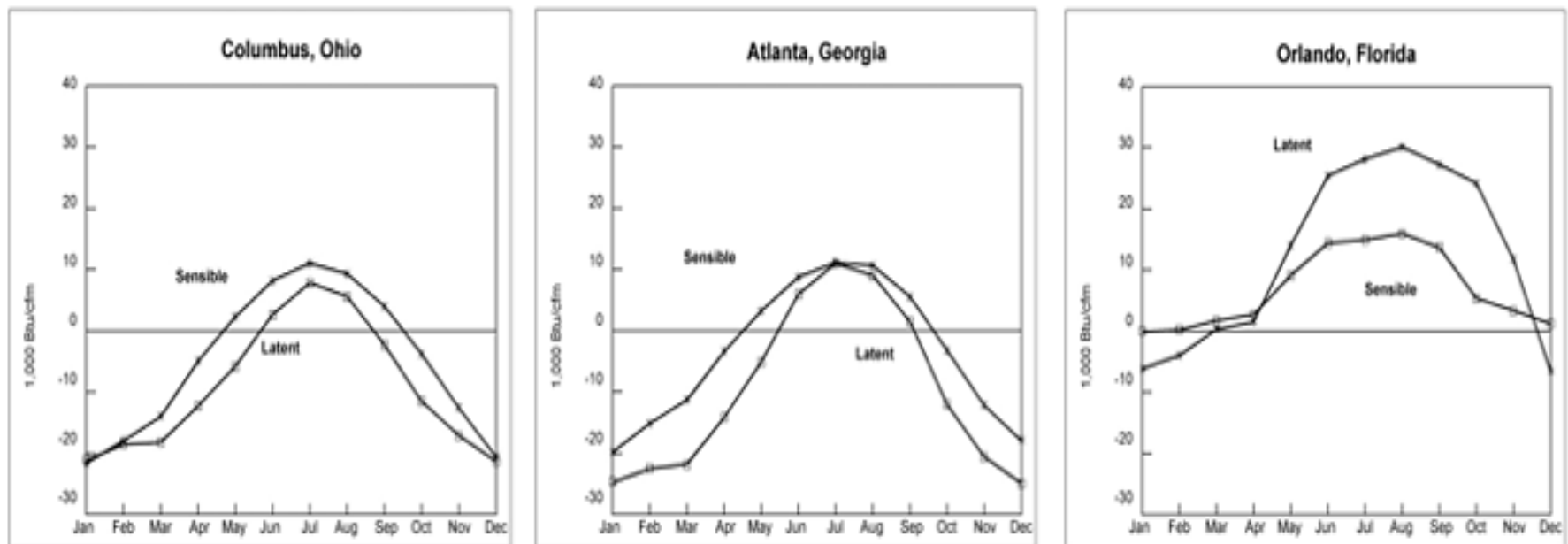


Cycle Analysis



Latent vs. Sensible Heat Load

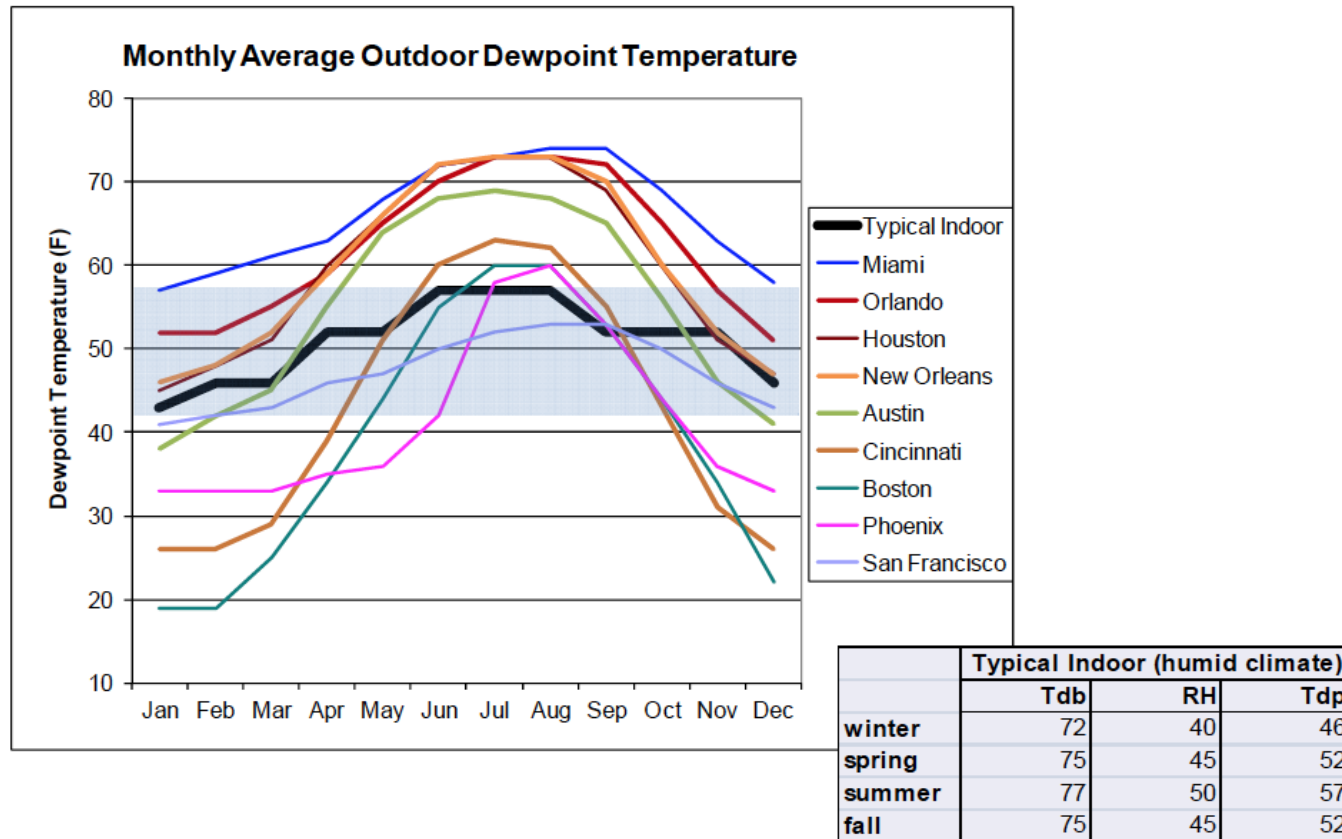
- Buildings latent heat significantly exceeds the sensible heat load in hot-humid climates



In Miami, the latent load exceeds the sensible load by 6.7:1

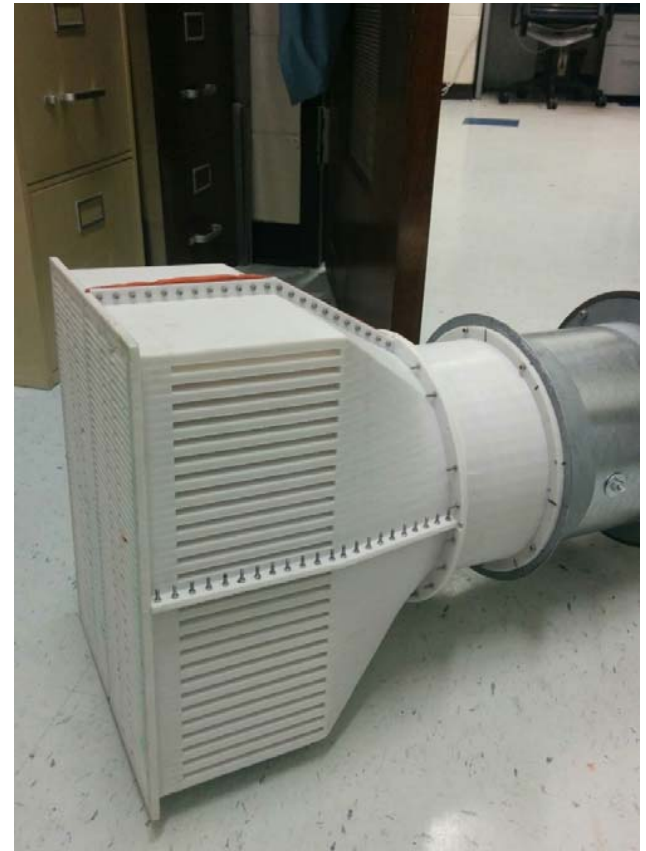
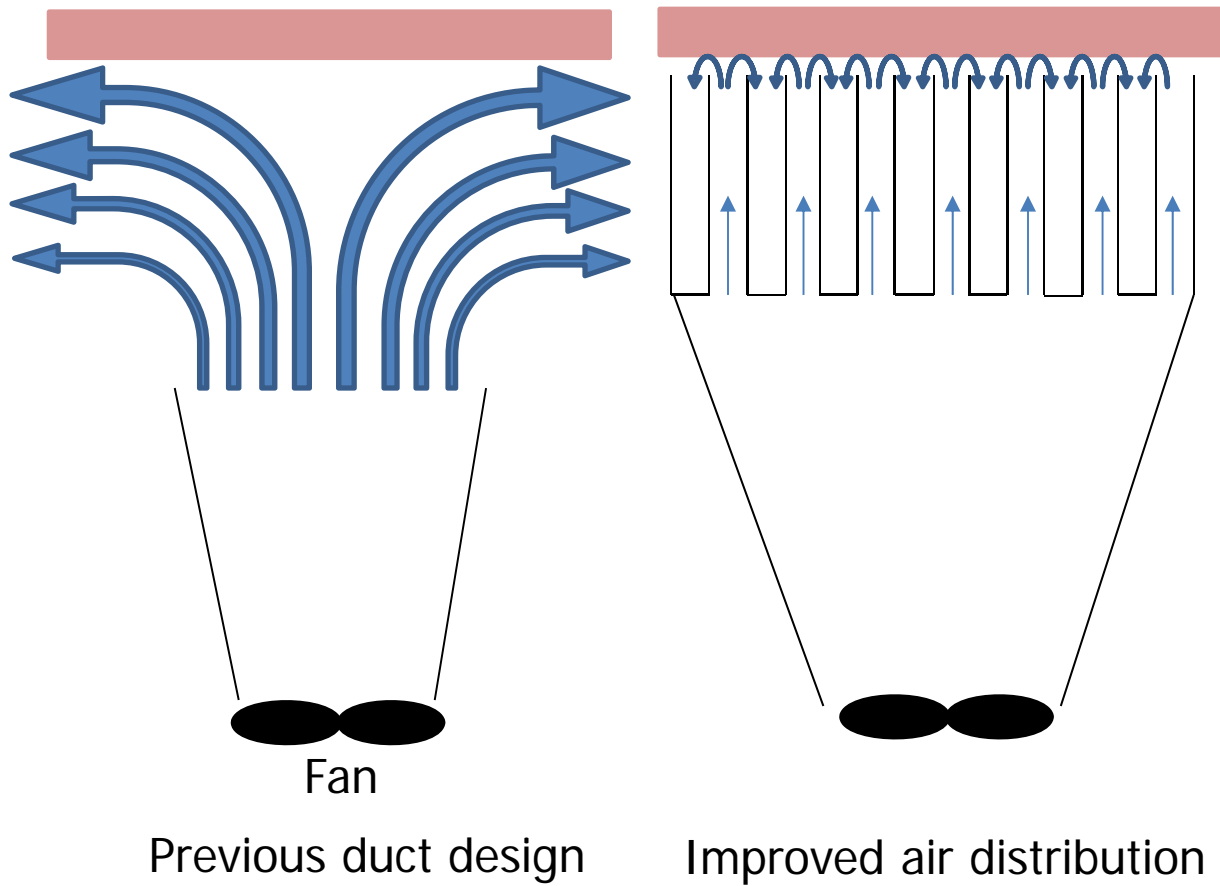
- ✓ Regional solutions

Humidity Control Challenges in Residential Buildings



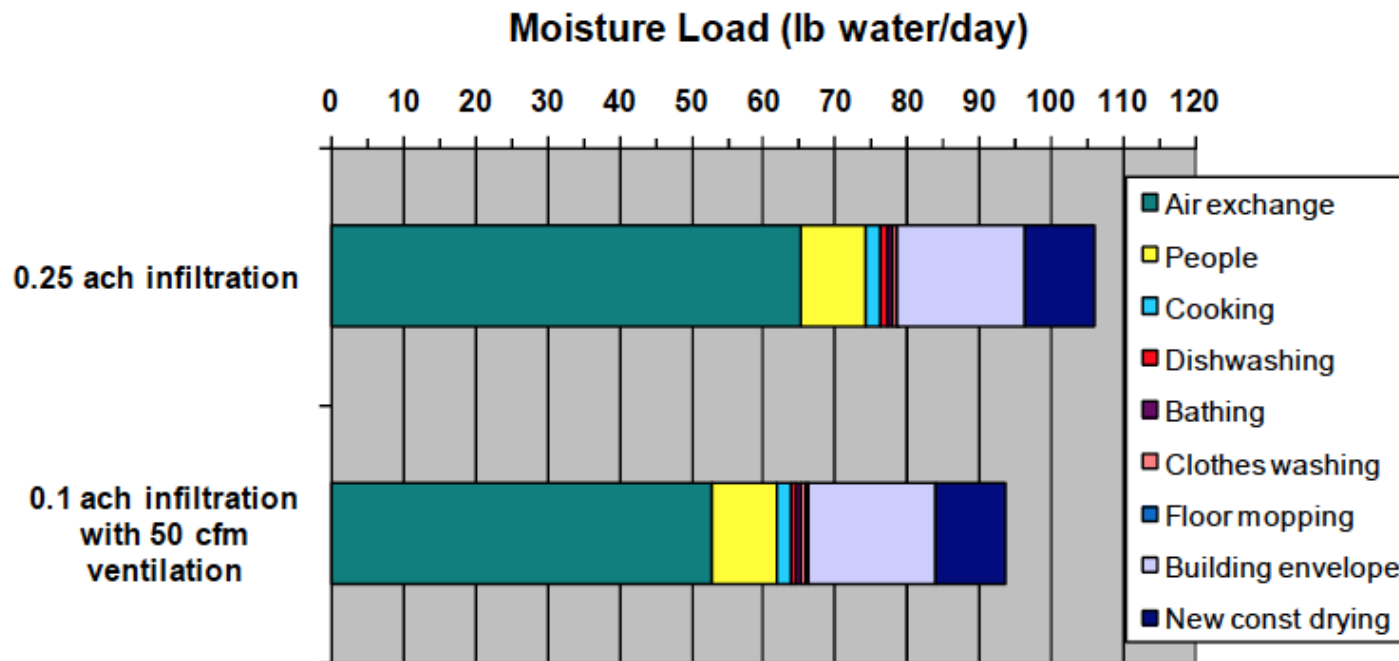
From: Armin Rudd, Residential Humidity Control Strategies, Residential Energy Efficiency Stakeholder Meeting, Austin TX, February 2012

Improvement of Air Distribution



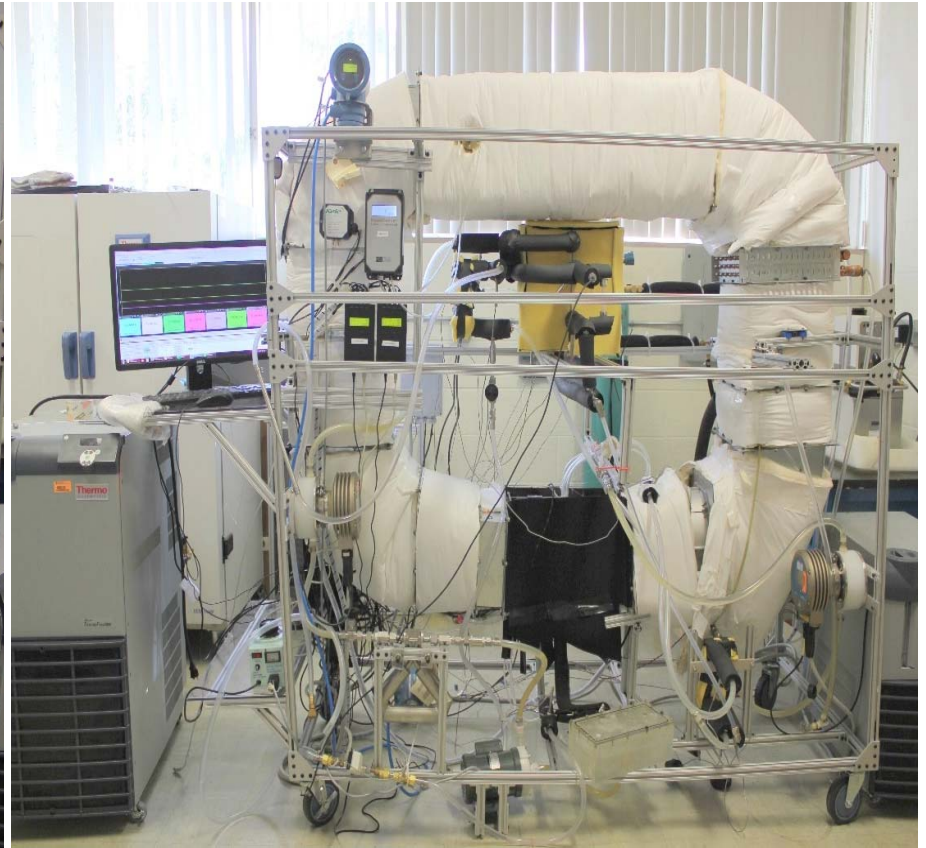
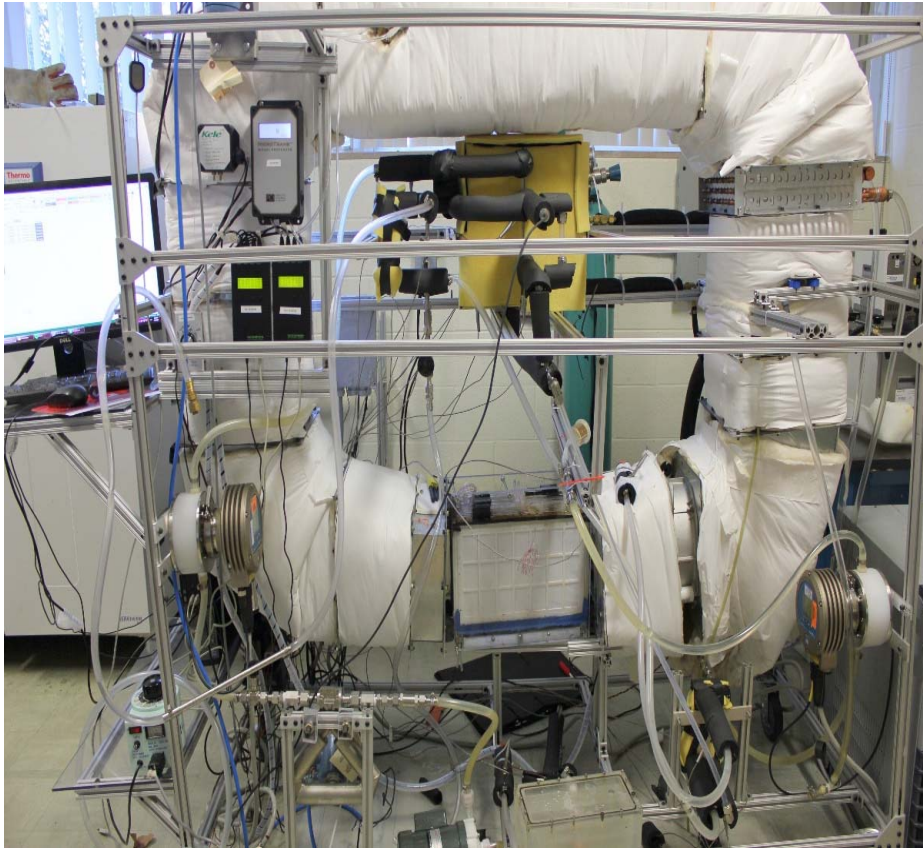
Humidity Control Challenges in Residential Buildings (cont.)

Moisture load for cooling and dehumidification systems
in humid climates (75 F/55% RH indoor, 75 F outdoor dewpt)



From: Armin Rudd, Residential Humidity Control Strategies, Residential Energy Efficiency Stakeholder Meeting, Austin TX, February 2012

Experimental Loop



Water Heater Configuration

